

148 River St., Suite 220, Greenville, SC 29601 | 864.421.9999

August 3, 2023

Ms. Salley Lewis Vulcan Materials Company 201 Brown Road Piedmont, SC 29673

Subject: Orangeburg Mine Map — Stormwater Runoff Design Summary

This letter and accompanying attachments provide guidelines for the design of two sediment basins (or detention ponds) at the Vulcan property located approximately 3 miles southeast from the city of Eutawville in Orangeburg County, South Carolina. The described measures are necessary to control sediment and stormwater runoff related to overburden area construction.

The overburden area at this project site is in the southwest portion of the property. A total of two sediment basins (or detention ponds) are needed because of the size of the overburden and topography of the area. The two basins/ponds are labeled as Pond 1 and Pond 2. Stormwater will be routed to the basins/ponds via ditches, terraces, and down drains.

The sediment basins are designed to treat stormwater from the overburden area by trapping sediment; the treated stormwater will be discharged downstream during construction. The location of the overburden area and sediment basins can be found on the Pre-Development and Post-Development Drainage Areas Figures (**Attachment 1**). The sediment produced from the overburden area will be routed to the two sediment basins. The sediment basins are designed to maintain a sediment trapping efficiency of at least 80 percent during a 25-year, 24-hour storm event.

After construction and stabilization at the project site, the sediment basins will be converted to detention ponds. The basins are designed to meet the detention pond criteria of not overtopping during a 100-year, 24-hour storm event, maintaining a minimum of 6 vertical inches between the water surface elevation and the emergency spillway during a 10-year, 24-hour storm event. The detention pond is designed to manage stormwater flows from the newly constructed areas designated on the grading plan.

Sediment, Erosion, Discharge by Computer-Aided Design (SEDCAD) hydrologic software was used to determine pre-development, during-construction (with sediment basins), and post-development (with detention ponds) stormwater runoff volumes and flow rates. As shown in the Sediment Basin and Detention Pond Parameters in **Attachment 2**, the peak flows at the hydrological points of interest meet the criteria of post-development peaks flows being less than pre-development peak flows for 2-year, 24-hour and 10-year, 24-hour storm events. The rainfall input data used to estimate storm flows in SEDCAD was provided by the South Carolina

Department of Health and Environmental Control (SCDHEC) Stormwater Management Best Management Practices Handbook.

The sediment basins and detention ponds have been designed to manage stormwater flows from the overburden area designated on the grading plans. The roadside ditch system and pipedown drains shown on the grading plans will allow for proper drainage to the ponds. **Attachment 2** titled Sediment Basin and Detention Pond Parameters describes the drainage areas, flow rates, and individual design guideline criteria for each of the ponds. The design guideline criteria for the basins/ponds are shown in the attached chart titled Sediment Basin and Detention Guidelines (**Attachment 3**). **Attachment 2** and **Attachment 3** are intended for field use. Pre-development, during-construction (with sediment basins), and post-development (with detention ponds) calculations from SEDCAD are included as **Attachment 4**.

The soil type around the pit area has a wide variety including, but not limited to Goldsboro sandy loam, Rains sandy loam, Lynchburg sandy loam, Stallings loamy sand, Coxville sandy loam, Mouzon fine sandy loam, Noboco sandy loam, and Ocilla loamy sand. The soil types carry a hydrologic soil group classification ranging from A to D, but overall, predominantly hydrologic soil group D. Pre-development ground cover is considered to be wooded in fair hydrologic condition and grassed in fair condition. The curve number representing wooded areas in fair condition is 79 and grassed in fair condition is 78. The post-development ground cover is considered to have fair grass cover with a curve number of 84. Impervious areas such as asphalt and buildings have a curve number of 98, and gravel areas have a curve number of 91. Some areas that contribute runoff to the hydrologic points of interest will remain undisturbed and will bypass the sediment ponds. Curve numbers for these areas are identical to pre-development conditions. A soil map is included as **Attachment 5**.

The following criteria will be identical for Pond 1 and Pond 2:

#### Concrete riser structure

- Minimum dimension of 48-inch diameter
- Trash rack
- Two floating skimmers
  - Skimmers will be removed, and the orifice will be plugged when the sediment ponds are converted to detention ponds.
  - $\circ$  Orifices will be installed when sediment ponds are converted to detention ponds.

### Rip-rap (SCDOT Class C) dike surrounding riser

- Number 5 stone on face
- Tie-in to earthen berm
- Minimum 5 feet distance between rip-rap and riser

#### Outlet pipe

- Concrete or corrugated metal
- Tie-in to riser

### Discharge location

- Rip-rap stone bed apron
- Filter fabric underlain and tied into adjacent grades
- Apron length and width adequate for proper energy dissipation

#### Berm designs

Each pond will have a:

- Minimum width of 25 feet
- Tie-in to existing ground
- 3 horizontal to 1 vertical side slope design

Best management practices — including, but not limited to, silt fence, stormwater ditching, and grassing — shall be used throughout the site during and after construction of the overburden areas to control erosion and/or off-site sedimentation.

Please review this information and respond with comments at your convenience.

Sincerely,

SynTerra

Lynna Lotrakul, P.E.

Senior Peer Review: udrea lehn

Andrea Kehn, P.E.

### **Attachments:**

Attachment 1	Pre-Development and Post-Development Drainage Areas Figures
Attachment 2	Sediment Basin and Detention Pond Parameters
Attachment 3	Sediment Basin and Detention Pond Construction Guidelines
Attachment 4	SEDCAD Output Reports
Attachment 5	Soil Map

#### Letter Orangeburg Ponds.docx

# **ATTACHMENT 1**

# PRE-DEVELOPMENT AND POST-DEVELOPMENT DRAINAGE AREAS FIGURES



# LEGEND:



OVERBURDEN AREA PROPERTY LINE ENTRANCE AND OFFICE AREA SHOP AREA PIT LIMIT BUFFER WETLANDS ARCHAEOLOGICAL SITE AREAS

PRE-DEVELOPMENT DRAINAGE AREA

- HYDROLOGIC POINT **OF INTEREST 4** 

HYDROLOGIC POINT OF INTEREST 3



PRE-DEVELOPMENT DRAINAGE AREAS

DATE 7/6/2023

ORANGEBURG QUARRY BY J. COLEMAN BY L. LOTRAKUL PROJ. NO. 00.5872.00 FILE SERVER 
 B
 DATE
 7/6/2023
 SCALE
 1" = 400'
 SHEET 1 OF 2



	Ε				TOLERANCES-UNLESS NOTED	
	D				FRACTIONAL: $\pm 1/16"$	
	С				ANGLE: ± 0.1°	
synierra	В				THIS DRAWING IN DESIGN AND DETAIL IS THE	
148 River Street, Suite 220 Greenville, South Carolina 29601	Α	7/6/2023	FOR CLIENT REVIEW	JCC	AND MUST BE RETURNED UPON DEMAND. THIS	Materials Company
864-421-9999 www.synterracorp.com		DATE	REVISION	BY	OR USED WITHOUT PERMISSION.	







# ATTACHMENT 2

# **SEDIMENT BASIN AND DETENTION POND PARAMETERS**

synterracorp.com

#### SEDIMENT BASIN AND DETENTION POND PARAMETERS

	Pre-Development Drainage Areas						
	POI 1	POI 2	POI 3	POI 4	TOTAL		
Existing Drainage Area (acre)	282.25	122.17	53.79	230.65	688.86		
		Doct Dov	alanmant Drai	Area			
	Post-Development Drainage Area						
	POI 1	POI 2	POI 3	POI 4	TOTAL		
Drainage Area towards POI (acre)	276.13	60.16	9.28	12.79	358.36		
Drainage Area towards Pit (acre)		330	).50		330.50		
Total (acre)					688.86		
	Pre-Development Flow Rates (cfs)						
Storm Event	POI 1						

Storm Event	POI 1	POI 2	POI 3	POI 4
2-year, 24-hour	76.76	99.01	21.69	97.47
10-year, 24-hour	153.51	152.36	43.22	196.96
25-year, 24-hour	206.15	186.92	57.90	265.22
100-year, 24-hour	297.20	245.32	83.22	383.45

	Post-Development Flow Rates (cfs)					
Storm Event	POI 1	POI 4				
2-year, 24-hour	31.00	15.28	12.33	4.72		
10-year, 24-hour	59.35	28.47	24.31	9.04		
25-year, 24-hour	78.21	37.06	32.40	11.96		
100-year, 24-hour	110.27	67.07	46.27	16.94		

	Basin/Pond Dimensions			
	Pond 1	Pond 1		
Bottom Elevation (ft)	89	86		
Top Elevation (ft)	96	96		
Depth (ft)	7	10		
Full Pond Surface Area (acre)	3.51	3.21		
	Emergenc	y Spillway		
Width (ft)	10	10		
Elevation (ft)	95	95		
	Charme Discor			
	3.011			
Top of Riser Elevation (ft)	93.5	93.5		
Skimmer Diameter* (in)	8	8		
Skimmer Orifice Elevation* (ft)	90	87		
Orifice Size** (in) and Elevation (ft)	8-inch at 89.5 f	8-inch at 86.5 ft		
Orifice Size** (in) and Elevation (ft)	-inch at 90.75	6-inch at 88.5 ft		
	Outle	t Pipe		
Diameter (in)	24	24		
Length (ft)	75	100		
Slope (%)	1.3	2.0		
Material	RCP	RCP		

#### Notes:

1. cfs = cubic feet per second

2. ft = feet

3. in = inches

4. POI = point of interest; refer to Pre-Development and Post-Development Drainage Areas Figures for locations

5. RCP = reinforced concrete pipe

6. (\*) For during construction. Two skimmers will be installed at each sediment basin.

7. (\*\*) For post construction/development

8. Sediment Basins will be converted to Detention Ponds for Post Construction/Development

# **ATTACHMENT 3**

# SEDIMENT BASIN AND DETENTION POND CONSTRUCTION GUIDELINES

## VULCAN QUARRIES - ORANGEBURG POND GENERAL CONSTRUCTION GUIDELINES



#### NOTES:

1. PONDS 1 AND 2 WILL BE LEFT AS PERMANENT DETENTION PONDS. THE SKIMMERS WILL BE REMOVED AND THE HOLES PATCHED. REFER TO THE TABLE BELOW FOR ORIFICE SIZES AND ELEVATIONS FOR THE STORM RISERS.

	DETENTION PONDS			
	1	2		
ORIFICE SIZE AND	8 IN AT			
CORRESPONDING				
ELEVATION	09.3 FI	00.3 FT		
ORIFICE SIZE AND				
CORRESPONDING				
ELEVATION	90.75 FT	88.5 FI		

# **ATTACHMENT 4**

# **SEDCAD OUTPUT REPORTS**

synterracorp.com

# **Vulcan Orangeburg**

Pre Development for Hydrological Point of Interest 1 through 4 2-year, 24-hour Storm Event 3.8 inches

L.Lotrakul

# **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	2 yr - 24 hr
Rainfall Depth:	3.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Null	#1	==>	#5	0.000	0.000	POI 1 (southwest)
Null	#2	==>	#5	0.000	0.000	POI 2 (most southern point)
Null	#3	==>	#5	0.000	0.000	POI 3 (mid south, from wetlands)
Null	#4	==>	#5	0.000	0.000	POI 4 (southeast)
Null	#5	==>	End	0.000	0.000	

# Structure Networking:

Æ	#4
	Null
Æ	#3
	Null
	#2
	Null
	#1
V	Null
#5	
Null	

	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
	(ac)	(ac)	(cfs)	(ac-ft)
#4	230.650	230.650	97.47	33.24
#3	53.790	53.790	21.69	8.01
#2	122.170	122.170	99.01	36.00
#1	282.250	282.250	76.76	42.04
#5	0.000	688.860	263.33	119.30

# Structure Summary:

# Structure Detail:

Structure #4 (Null)

POI 4 (southeast)

Structure #3 (Null)

POI 3 (mid south, from wetlands)

Structure #2 (Null)

POI 2 (most southern point)

Structure #1 (Null)

POI 1 (southwest)

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	157.970	2.178	1.122	0.130	78.000	TR55	83.71	22.575
	2	72.680	5.300	0.000	0.000	78.640	TR55	20.32	10.666
	Σ	230.650						97.47	33.241
#3	1	53.790	3.363	0.000	0.000	79.000	TR55	21.69	8.013
	Σ	53.790						21.69	8.013
#2	1	122.170	3.144	0.000	0.000	98.000	TR55	99.01	36.000
	Σ	122.170						99.01	36.000
#1	1	282.250	5.614	0.000	0.000	79.000	TR55	76.76	42.044
	Σ	282.250						76.76	42.044
#5	Σ	688.860						263.33	119.298

# Subwatershed Hydrology Detail:

# Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	1. Forest with heavy ground litter	1.05	2.00	191.00	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,340.00	0.110	16.010
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.00	0.720	0.657
#1	1	Time of Concentration:					5.614
#2	1	1. Forest with heavy ground litter	0.37	0.50	135.00	0.150	0.250
		4. Cultivated, straight row	0.09	2.00	2,265.00	0.260	2.419
		4. Cultivated, straight row	0.41	2.00	482.00	0.570	0.234
		8. Large gullies, diversions, and low flowing streams	0.11	1.00	879.00	1.010	0.241
#2	1	Time of Concentration:					3.144
#3	1	1. Forest with heavy ground litter	0.66	1.00	151.00	0.200	0.209
		4. Cultivated, straight row	0.05	1.00	2,141.00	0.190	3.130
		8. Large gullies, diversions, and low flowing streams	0.53	1.00	190.00	2.170	0.024
#3	1	Time of Concentration:					3.363
#4	1	1. Forest with heavy ground litter	20.59	7.00	34.00	1.140	0.008
		8. Large gullies, diversions, and low flowing streams	0.04	2.00	4,767.00	0.610	2.170
#4	1	Time of Concentration:					2.178
#4	2	8. Large gullies, diversions, and low flowing streams	0.02	1.00	5,866.00	0.390	4.178
		8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122

## **SEDCAD 4 for Windows**

Convright 1008 -2010 Pamela I Schwah

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	2	Time of Concentration:					5.300

# Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122
#4	1	Muskingum K:					1.122

# **Vulcan Orangeburg**

*Pre Development for Hydrological Point of Interest 1 through 4 10-year, 24-hour Storm Event 5.8 inches* 

L.Lotrakul

# **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Null	#1	==>	#5	0.000	0.000	POI 1 (southwest)
Null	#2	==>	#5	0.000	0.000	POI 2 (most southern point)
Null	#3	==>	#5	0.000	0.000	POI 3 (mid south, from wetlands)
Null	#4	==>	#5	0.000	0.000	POI 4 (southeast)
Null	#5	==>	End	0.000	0.000	

# Structure Networking:

Æ	#4
~	Null
Æ	#3
$\sim$	Null
	#2
	Null
Æ	#1
	Null
#5	
Null	

	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
	(ac)	(ac)	(cfs)	(ac-ft)
#4	230.650	230.650	196.96	65.25
#3	53.790	53.790	43.22	15.57
#2	122.170	122.170	152.36	56.16
#1	282.250	282.250	153.51	81.68
#5	0.000	688.860	492.64	218.65

# Structure Summary:

# Structure Detail:

Structure #4 (Null)

POI 4 (southeast)

Structure #3 (Null)

POI 3 (mid south, from wetlands)

Structure #2 (Null)

POI 2 (most southern point)

Structure #1 (Null)

POI 1 (southwest)

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	157.970	2.178	1.122	0.130	78.000	TR55	169.01	44.432
	2	72.680	5.300	0.000	0.000	78.640	TR55	40.88	20.818
	Σ	230.650						196.96	65.250
#3	1	53.790	3.363	0.000	0.000	79.000	TR55	43.22	15.567
	Σ	53.790						43.22	15.567
#2	1	122.170	3.144	0.000	0.000	98.000	TR55	152.36	56.157
	Σ	122.170						152.36	56.157
#1	1	282.250	5.614	0.000	0.000	79.000	TR55	153.51	81.681
	Σ	282.250						153.51	81.681
#5	Σ	688.860						492.64	218.654

# Subwatershed Hydrology Detail:

# Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	1. Forest with heavy ground litter	1.05	2.00	191.00	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,340.00	0.110	16.010
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.00	0.720	0.657
#1	1	Time of Concentration:					5.614
#2	1	1. Forest with heavy ground litter	0.37	0.50	135.00	0.150	0.250
		4. Cultivated, straight row	0.09	2.00	2,265.00	0.260	2.419
		4. Cultivated, straight row	0.41	2.00	482.00	0.570	0.234
		8. Large gullies, diversions, and low flowing streams	0.11	1.00	879.00	1.010	0.241
#2	1	Time of Concentration:					3.144
#3	1	1. Forest with heavy ground litter	0.66	1.00	151.00	0.200	0.209
		4. Cultivated, straight row	0.05	1.00	2,141.00	0.190	3.130
		8. Large gullies, diversions, and low flowing streams	0.53	1.00	190.00	2.170	0.024
#3	1	Time of Concentration:					3.363
#4	1	1. Forest with heavy ground litter	20.59	7.00	34.00	1.140	0.008
		8. Large gullies, diversions, and low flowing streams	0.04	2.00	4,767.00	0.610	2.170
#4	1	Time of Concentration:					2.178
#4	2	8. Large gullies, diversions, and low flowing streams	0.02	1.00	5,866.00	0.390	4.178
		8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122

## **SEDCAD 4 for Windows**

Convright 1008 -2010 Pamela I. Schwah

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	2	Time of Concentration:					5.300

# Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122
#4	1	Muskingum K:					1.122

# **Vulcan Orangeburg**

*Pre Development for Hydrological Point of Interest 1 through 4 25-year, 24-hour Storm Event 7.1 inches* 

L.Lotrakul

# **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Null	#1	==>	#5	0.000	0.000	POI 1 (southwest)
Null	#2	==>	#5	0.000	0.000	POI 2 (most southern point)
Null	#3	==>	#5	0.000	0.000	POI 3 (mid south, from wetlands)
Null	#4	==>	#5	0.000	0.000	POI 4 (southeast)
Null	#5	==>	End	0.000	0.000	

# Structure Networking:

Æ	#4
~	Null
Æ	#3
	Null
	#2
	Null
Æ	#1
	Null
#5	
Null	

	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
	(ac)	(ac)	(cfs)	(ac-ft)
#4	230.650	230.650	265.22	87.46
#3	53.790	53.790	57.90	20.79
#2	122.170	122.170	186.92	69.27
#1	282.250	282.250	206.15	109.08
#5	0.000	688.860	648.73	286.60

# Structure Summary:

# Structure Detail:

Structure #4 (Null)

POI 4 (southeast)

Structure #3 (Null)

POI 3 (mid south, from wetlands)

Structure #2 (Null)

POI 2 (most southern point)

Structure #1 (Null)

POI 1 (southwest)

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	157.970	2.178	1.122	0.130	78.000	TR55	227.56	59.615
	2	72.680	5.300	0.000	0.000	78.640	TR55	55.00	27.848
	Σ	230.650						265.22	87.462
#3	1	53.790	3.363	0.000	0.000	79.000	TR55	57.90	20.788
	Σ	53.790						57.90	20.788
#2	1	122.170	3.144	0.000	0.000	98.000	TR55	186.92	69.269
	Σ	122.170						186.92	69.269
#1	1	282.250	5.614	0.000	0.000	79.000	TR55	206.15	109.076
	Σ	282.250						206.15	109.076
#5	Σ	688.860						648.73	286.595

# Subwatershed Hydrology Detail:

# Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	1. Forest with heavy ground litter	1.05	2.00	191.00	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,340.00	0.110	16.010
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.00	0.720	0.657
#1	1	Time of Concentration:					5.614
#2	1	1. Forest with heavy ground litter	0.37	0.50	135.00	0.150	0.250
		4. Cultivated, straight row	0.09	2.00	2,265.00	0.260	2.419
		4. Cultivated, straight row	0.41	2.00	482.00	0.570	0.234
		8. Large gullies, diversions, and low flowing streams	0.11	1.00	879.00	1.010	0.241
#2	1	Time of Concentration:					3.144
#3	1	1. Forest with heavy ground litter	0.66	1.00	151.00	0.200	0.209
		4. Cultivated, straight row	0.05	1.00	2,141.00	0.190	3.130
		8. Large gullies, diversions, and low flowing streams	0.53	1.00	190.00	2.170	0.024
#3	1	Time of Concentration:					3.363
#4	1	1. Forest with heavy ground litter	20.59	7.00	34.00	1.140	0.008
		8. Large gullies, diversions, and low flowing streams	0.04	2.00	4,767.00	0.610	2.170
#4	1	Time of Concentration:					2.178
#4	2	8. Large gullies, diversions, and low flowing streams	0.02	1.00	5,866.00	0.390	4.178
		8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122

## **SEDCAD 4 for Windows**

Convright 1008 -2010 Pamela I. Schwah

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	2	Time of Concentration:					5.300

# Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122
#4	1	Muskingum K:					1.122

# **Vulcan Orangeburg**

*Pre Development for Hydrological Point of Interest 1 through 4 100-year, 24-hour Storm Event 9.3 inches* 

L.Lotrakul

# **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Null	#1	==>	#5	0.000	0.000	POI 1 (southwest)
Null	#2	==>	#5	0.000	0.000	POI 2 (most southern point)
Null	#3	==>	#5	0.000	0.000	POI 3 (mid south, from wetlands)
Null	#4	==>	#5	0.000	0.000	POI 4 (southeast)
Null	#5	==>	End	0.000	0.000	

# Structure Networking:

Æ	#4			
~	Null			
Æ	#3			
	Null			
	#2			
	Null			
Æ	#1			
	Null			
#5				
Null				
	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
----	-----------------------------------	-------------------------------	-------------------	---------------------------
	(ac)	(ac)	(cfs)	(ac-ft)
#4	230.650	230.650	383.45	126.37
#3	53.790	53.790	83.22	29.91
#2	122.170	122.170	245.32	91.47
#1	282.250	282.250	297.20	156.96
#5	0.000	688.860	917.86	404.71

### Structure Summary:

### Structure Detail:

Structure #4 (Null)

POI 4 (southeast)

Structure #3 (Null)

POI 3 (mid south, from wetlands)

Structure #2 (Null)

POI 2 (most southern point)

Structure #1 (Null)

POI 1 (southwest)

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	157.970	2.178	1.122	0.130	78.000	TR55	328.61	86.227
	2	72.680	5.300	0.000	0.000	78.640	TR55	79.44	40.146
	Σ	230.650						383.45	126.373
#3	1	53.790	3.363	0.000	0.000	79.000	TR55	83.22	29.913
	Σ	53.790						83.22	29.913
#2	1	122.170	3.144	0.000	0.000	98.000	TR55	245.32	91.468
	Σ	122.170						245.32	91.468
#1	1	282.250	5.614	0.000	0.000	79.000	TR55	297.20	156.955
	Σ	282.250						297.20	156.955
#5	Σ	688.860						917.86	404.709

### Subwatershed Hydrology Detail:

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	1. Forest with heavy ground litter	1.05	2.00	191.00	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,340.00	0.110	16.010
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.00	0.720	0.657
#1	1	Time of Concentration:					5.614
#2	1	1. Forest with heavy ground litter	0.37	0.50	135.00	0.150	0.250
		4. Cultivated, straight row	0.09	2.00	2,265.00	0.260	2.419
		4. Cultivated, straight row	0.41	2.00	482.00	0.570	0.234
		8. Large gullies, diversions, and low flowing streams	0.11	1.00	879.00	1.010	0.241
#2	1	Time of Concentration:					3.144
#3	1	1. Forest with heavy ground litter	0.66	1.00	151.00	0.200	0.209
		4. Cultivated, straight row	0.05	1.00	2,141.00	0.190	3.130
		8. Large gullies, diversions, and low flowing streams	0.53	1.00	190.00	2.170	0.024
#3	1	Time of Concentration:					3.363
#4	1	1. Forest with heavy ground litter	20.59	7.00	34.00	1.140	0.008
		8. Large gullies, diversions, and low flowing streams	0.04	2.00	4,767.00	0.610	2.170
#4	1	Time of Concentration:					2.178
#4	2	8. Large gullies, diversions, and low flowing streams	0.02	1.00	5,866.00	0.390	4.178
		8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122

### **SEDCAD 4 for Windows**

Convright 1008 -2010 Pamela I. Schwah

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	2	Time of Concentration:					5.300

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	8. Large gullies, diversions, and low flowing streams	0.04	1.00	2,425.00	0.600	1.122
#4	1	Muskingum K:					1.122

# **Vulcan Orangeburg**

During Construction Sediment Basin 1 10-year, 24-hour Storm Event 5.8 inches

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

### Particle Size Distribution:

Size (mm)	Coxville
1.4000	100.000%
1.0000	89.600%
0.0630	65.700%
0.0440	43.900%
0.0380	42.400%
0.0040	5.000%
0.0030	3.100%
0.0010	0.000%

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#6	0.000	0.000	Temp. Sed. Pond
Null	#6	==>	End	0.000	0.000	





		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc. (ml/l)	24VW (ml/l)
#1	In	38 420	38 420	249.31	16.53	12,223.7	797,047	492.06	255.14
#1	Out	30.420	50.420	9.91	11.11	624.5	161,751	0.04	0.02
#6		0.000	38.420	9.91	11.11	624.5	161,689	0.04	0.02

### Structure Summary:

## Particle Size Distribution(s) at Each Structure

Size (mm)	In	Out
1.4000	100.000%	100.000%
1.0000	99.034%	100.000%
0.0630	72.617%	100.000%
0.0440	48.522%	100.000%
0.0380	46.864%	100.000%
0.0040	5.526%	100.000%
0.0030	3.426%	67.062%
0.0010	0.000%	0.000%

### Structure #1 (Temp. Sed. Pond ):

Structu	re #6:
Size (mm)	In/Out
1.4000	100.000%
1.0000	100.000%

1.4000	100.000 /0
1.0000	100.000%
0.0630	100.000%
0.0440	100.000%
0.0380	100.000%
0.0040	100.000%
0.0030	67.062%
0.0010	0.000%

### Structure Detail:

#### Structure #1 (Pond)

Temp. Sed. Pond

Pond Inputs:

Initial Pool Elev:	89.50 ft
Initial Pool:	0.68 ac-ft
*Sediment Storage:	0.00 ac-ft
Dead Space:	0.00 %

\*No sediment capacity defined

### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	5.00	24.00	75.00	1.30	0.0150	93.50	4

### **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	93.78 ft
H'graph Detention Time:	12.16 hrs
Pond Model:	CSTRS
Dewater Time:	3.83 days
Trap Efficiency:	94.89 %

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

## SEDCAD 4 for Windows Convright 1998 - 2010 Pamela I. Schwab

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		Top of Sed. Storage
89.01	1.102	0.011	0.000		
89.50	1.634	0.677	0.000		
90.00	2.284	1.652	2.260	5.22*	
90.01	2.286	1.675	2.260	0.12*	
90.50	2.381	2.818	2.260	6.12*	
91.00	2.480	4.033	2.260	6.51*	
91.50	2.580	5.298	2.260	6.77*	
92.00	2.683	6.614	2.260	7.04*	
92.50	2.782	7.980	2.260	7.31*	
93.00	2.882	9.395	2.260	7.58*	
93.50	2.984	10.862	2.260	7.85*	Spillway #2
93.78	3.042	11.705	9.912	36.15	Peak Stage
94.00	3.088	12.380	16.033		
94.50	3.190	13.949	36.688		
95.00	3.293	15.570	37.901		Spillway #3
95.50	3.398	17.243	51.150		
96.00	3.505	18.968	64.363		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

### Detailed Discharge Table

		llcer-			Combined
Elevation	User-	Enh. PerfRiser	nh. PerfRiser Emergency		Total
(ft)	input discharge (cfs)	(cfs)	Spillway (cfs)	input discharge (cfs)	Discharge
	(0.0)			(0.0)	(cfs)
89.00	0.000	0.000	0.000	0.000	0.000
89.01	0.000	0.000	0.000	0.000	0.000
89.50	0.000	0.000	0.000	0.000	0.000
90.00	1.130	0.000	0.000	1.130	2.260
90.01	1.130	0.000	0.000	1.130	2.260
90.50	1.130	0.000	0.000	1.130	2.260
91.00	1.130	0.000	0.000	1.130	2.260
91.50	1.130	0.000	0.000	1.130	2.260
92.00	1.130	0.000	0.000	1.130	2.260
92.50	1.130	0.000	0.000	1.130	2.260
93.00	1.130	0.000	0.000	1.130	2.260
93.50	1.130	0.000	0.000	1.130	2.260
94.00	1.130	13.773	0.000	1.130	16.033
94.50	1.130	34.428	0.000	1.130	36.688
95.00	1.130	35.641	0.000	1.130	37.901
95.50	1.130	36.813	12.076	1.130	51.150

## SEDCAD 4 for Windows

Elevation (ft)	User- input discharge (cfs)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
96.00	1.130	37.950	24.153	1.130	64.363

Structure #6 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	38.420	0.171	0.000	0.000	94.000	TR55	249.31	16.529
	Σ	38.420						249.31	16.529
#6	Σ	38.420						9.91	11.111

## Subwatershed Hydrology Detail:

## Subwatershed Sedimentology Detail:

Stru #	SWS #	Soil K	L (ft)	S (%)	С	Ρ	PS #	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc (ml/l)	24VW (ml/l)
#1	1	0.240	1,402.00	10.00	1.0000	1.0000	1	12,223.7	797,047	492.06	255.14
	Σ							12,223.7	797,047	492.06	255.14
#6	Σ							624.5	161,689	0.04	0.02

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171

# **Vulcan Orangeburg**

During Construction Sediment Basin 1 25-year, 24-hour Storm Event 7.1 inches

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

### Particle Size Distribution:

Size (mm)	Coxville
1.4000	100.000%
1.0000	89.600%
0.0630	65.700%
0.0440	43.900%
0.0380	42.400%
0.0040	5.000%
0.0030	3.100%
0.0010	0.000%

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#6	0.000	0.000	Temp. Sed. Pond
Null	#6	==>	End	0.000	0.000	





		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc. (ml/l)	24VW (ml/l)						
#1	In	38 420	38 420	308.46	20.71	15,624.2	811,535	501.08	258.96						
	Out	30.420	38.420	50.720	30.420	30.420	36.420	50.420	36.420	J0.720 J0.720	26.62	15.24	1,293.4	164,542	24.95
#6		0.000	38.420	26.62	15.24	1,293.4	164,479	24.94	11.97						

### Structure Summary:

## Particle Size Distribution(s) at Each Structure

Size (mm)	In	Out
1.4000	100.000%	100.000%
1.0000	98.973%	100.000%
0.0630	72.573%	100.000%
0.0440	48.492%	100.000%
0.0380	46.835%	100.000%
0.0040	5.523%	66.717%
0.0030	3.424%	41.365%
0.0010	0.000%	0.000%

### Structure #1 (Temp. Sed. Pond ):

Str	'UC	tur	e #	<b>:6</b> :

Size (mm)	In/Out
1.4000	100.000%
1.0000	100.000%
0.0630	100.000%
0.0440	100.000%
0.0380	100.000%
0.0040	66.717%
0.0030	41.365%
0.0010	0.000%

### Structure Detail:

#### Structure #1 (Pond)

Temp. Sed. Pond

Pond Inputs:

Initial Pool Elev:	89.50 ft
Initial Pool:	0.68 ac-ft
*Sediment Storage:	0.00 ac-ft
Dead Space:	0.00 %

\*No sediment capacity defined

### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	5.00	24.00	75.00	1.30	0.0150	93.50	4

### **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev Crest Length (ft)		Left	Right	Bottom
		Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	94.26 ft
H'graph Detention Time:	9.32 hrs
Pond Model:	CSTRS
Dewater Time:	2.39 days
Trap Efficiency:	91.72 %

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

## SEDCAD 4 for Windows Convright 1998 - 2010 Pamela I. Schwab

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		Top of Sed. Storage
89.01	1.102	0.011	0.000		
89.50	1.634	0.677	0.000		
90.00	2.284	1.652	2.260	5.22*	
90.01	2.286	1.675	2.260	0.12*	
90.50	2.381	2.818	2.260	6.12*	
91.00	2.480	4.033	2.260	6.51*	
91.50	2.580	5.298	2.260	6.77*	
92.00	2.683	6.614	2.260	7.04*	
92.50	2.782	7.980	2.260	7.31*	
93.00	2.882	9.395	2.260	7.58*	
93.50	2.984	10.862	2.260	7.85*	Spillway #2
94.00	3.088	12.380	16.033	1.15*	
94.26	3.140	13.184	26.618	1.60	Peak Stage
94.50	3.190	13.949	36.688		
95.00	3.293	15.570	37.901		Spillway #3
95.50	3.398	17.243	51.150		
96.00	3.505	18.968	64.363		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

### Detailed Discharge Table

					Combined
Elevation	User-	Enh. PerfRiser	Emergency	User-	Total
(ft)	input discharge (cfs)	(cfs)	Spillway (cfs)	input discharge (cfs)	Discharge
	(013)			(013)	(cfs)
89.00	0.000	0.000	0.000	0.000	0.000
89.01	0.000	0.000	0.000	0.000	0.000
89.50	0.000	0.000	0.000	0.000	0.000
90.00	1.130	0.000	0.000	1.130	2.260
90.01	1.130	0.000	0.000	1.130	2.260
90.50	1.130	0.000	0.000	1.130	2.260
91.00	1.130	0.000	0.000	1.130	2.260
91.50	1.130	0.000	0.000	1.130	2.260
92.00	1.130	0.000	0.000	1.130	2.260
92.50	1.130	0.000	0.000	1.130	2.260
93.00	1.130	0.000	0.000	1.130	2.260
93.50	1.130	0.000	0.000	1.130	2.260
94.00	1.130	13.773	0.000	1.130	16.033
94.50	1.130	34.428	0.000	1.130	36.688
95.00	1.130	35.641	0.000	1.130	37.901
95.50	1.130	36.813	12.076	1.130	51.150

## SEDCAD 4 for Windows

Elevation (ft)	User- input discharge (cfs)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
96.00	1.130	37.950	24.153	1.130	64.363

Structure #6 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	38.420	0.171	0.000	0.000	94.000	TR55	308.46	20.708
	Σ	38.420						308.46	20.708
#6	Σ	38.420						26.62	15.239

## Subwatershed Hydrology Detail:

## Subwatershed Sedimentology Detail:

Stru #	SWS #	Soil K	L (ft)	S (%)	С	Ρ	PS #	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc (ml/l)	24VW (ml/l)
#1	1	0.240	1,402.00	10.00	1.0000	1.0000	1	15,624.2	811,535	501.08	258.96
	Σ							15,624.2	811,535	501.08	258.96
#6	Σ							1,293.4	164,479	24.94	11.97

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171

# **Vulcan Orangeburg**

During Construction Sediment Basin 1 100-year, 24-hour Storm Event 9.3 inches

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

### Particle Size Distribution:

Size (mm)	Coxville
1.4000	100.000%
1.0000	89.600%
0.0630	65.700%
0.0440	43.900%
0.0380	42.400%
0.0040	5.000%
0.0030	3.100%
0.0010	0.000%

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#6	0.000	0.000	Temp. Sed. Pond
Null	#6	==>	End	0.000	0.000	





		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc. (ml/l)	24VW (ml/l)
#1	In	38 420	38 420	407.96	27.80	21,549.3	830,862	513.10	264.16
#1	41 56.420 56.420 Out	48.63	22.26	2,503.4	172,336	42.90	23.75		
#6		0.000	38.420	48.63	22.26	2,503.4	172,269	42.88	23.74

### Structure Summary:

## Particle Size Distribution(s) at Each Structure

Size (mm)	In	Out
1.4000	100.000%	100.000%
1.0000	98.915%	100.000%
0.0630	72.530%	100.000%
0.0440	48.464%	100.000%
0.0380	46.808%	100.000%
0.0040	5.520%	47.514%
0.0030	3.422%	29.459%
0.0010	0.000%	0.000%

### Structure #1 (Temp. Sed. Pond ):

Struct	ure #6:	
Size (mm)	In/Out	

Size (mm)	In/Out
1.4000	100.000%
1.0000	100.000%
0.0630	100.000%
0.0440	100.000%
0.0380	100.000%
0.0040	47.514%
0.0030	29.459%
0.0010	0.000%

### Structure Detail:

#### Structure #1 (Pond)

Temp. Sed. Pond

Pond Inputs:

Initial Pool Elev:	89.50 ft
Initial Pool:	0.68 ac-ft
*Sediment Storage:	0.00 ac-ft
Dead Space:	0.00 %

\*No sediment capacity defined

### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	5.00	24.00	75.00	1.30	0.0150	93.50	4

### **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	95.40 ft
H'graph Detention Time:	7.03 hrs
Pond Model:	CSTRS
Dewater Time:	2.46 days
Trap Efficiency:	88.38 %

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

## SEDCAD 4 for Windows Convright 1998 - 2010 Pamela I. Schwab

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		Top of Sed. Storage
89.01	1.102	0.011	0.000		
89.50	1.634	0.677	0.000		
90.00	2.284	1.652	2.260	5.22*	
90.01	2.286	1.675	2.260	0.12*	
90.50	2.381	2.818	2.260	6.12*	
91.00	2.480	4.033	2.260	6.51*	
91.50	2.580	5.298	2.260	6.77*	
92.00	2.683	6.614	2.260	7.04*	
92.50	2.782	7.980	2.260	7.31*	
93.00	2.882	9.395	2.260	7.58*	
93.50	2.984	10.862	2.260	7.85*	Spillway #2
94.00	3.088	12.380	16.033	1.15*	
94.50	3.190	13.949	36.688	1.45	
95.00	3.293	15.570	37.901	0.85	Spillway #3
95.40	3.378	16.924	48.625	1.00	Peak Stage
95.50	3.398	17.243	51.150		
96.00	3.505	18.968	64.363		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

### Detailed Discharge Table

	Licor-				Combined
Elevation	User-	Enh. PerfRiser	Emergency	User-	Total
(ft)	input discharge (cfs)	(cfs)	Spillway (cfs)	input discharge (cfs)	Discharge
	(0.0)			(0.0)	(cfs)
89.00	0.000	0.000	0.000	0.000	0.000
89.01	0.000	0.000	0.000	0.000	0.000
89.50	0.000	0.000	0.000	0.000	0.000
90.00	1.130	0.000	0.000	1.130	2.260
90.01	1.130	0.000	0.000	1.130	2.260
90.50	1.130	0.000	0.000	1.130	2.260
91.00	1.130	0.000	0.000	1.130	2.260
91.50	1.130	0.000	0.000	1.130	2.260
92.00	1.130	0.000	0.000	1.130	2.260
92.50	1.130	0.000	0.000	1.130	2.260
93.00	1.130	0.000	0.000	1.130	2.260
93.50	1.130	0.000	0.000	1.130	2.260
94.00	1.130	13.773	0.000	1.130	16.033
94.50	1.130	34.428	0.000	1.130	36.688
95.00	1.130	35.641	0.000	1.130	37.901
95.50	1.130	36.813	12.076	1.130	51.150

## SEDCAD 4 for Windows

Elevation (ft)	User- input discharge (cfs)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
96.00	1.130	37.950	24.153	1.130	64.363

Structure #6 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	38.420	0.171	0.000	0.000	94.000	TR55	407.96	27.802
	Σ	38.420						407.96	27.802
#6	Σ	38.420						48.63	22.264

## Subwatershed Hydrology Detail:

## Subwatershed Sedimentology Detail:

Stru #	SWS #	Soil K	L (ft)	S (%)	С	Ρ	PS #	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc (ml/l)	24VW (ml/l)
#1	1	0.240	1,402.00	10.00	1.0000	1.0000	1	21,549.3	830,862	513.10	264.16
	Σ							21,549.3	830,862	513.10	264.16
#6	Σ							2,503.4	172,269	42.88	23.74

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171

# **Vulcan Orangeburg**

During Construction Sediment Basin 2 10-year, 24-hour storm event 5.8 inches

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

### Particle Size Distribution:

Size (mm)	Coxville
1.4000	100.000%
1.0000	89.600%
0.0630	65.700%
0.0440	43.900%
0.0380	42.400%
0.0040	5.000%
0.0030	3.100%
0.0010	0.000%

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#5	4.810	0.162	Sediment Basin 2
Null	#5	==>	End	0.000	0.000	





## Structure Routing Details:

Stru #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	8. Large gullies, diversions, and low flowing streams	0.93	4.00	432.00	2.88	0.041
	1. Forest with heavy ground litter	0.08	1.00	1,202.00	0.07	4.769
#1	Muskingum K:					4.810

		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc. (ml/l)	24VW (ml/l)
#1	In	44 210	44.210	287.77	19.05	1,305.1	103,977	64.22	30.19
#1	Out	44.210		2.26	8.21	40.2	20,080	0.00	0.00
#5		0.000	44.210	2.26	8.21	40.2	1,949,172	0.08	0.00

### Structure Summary:

## Particle Size Distribution(s) at Each Structure

Size (mm)	In	Out
1.4000	100.000%	100.000%
1.0000	98.863%	100.000%
0.0630	72.492%	100.000%
0.0440	48.438%	100.000%
0.0380	46.783%	100.000%
0.0040	5.517%	100.000%
0.0030	3.420%	100.000%
0.0010	0.000%	0.000%

### Structure #1 (Sediment Basin 2 ):

Str	UC	tur	е	#5	5,

Size (mm)	In/Out
1.4000	100.000%
1.0000	100.000%
0.0630	100.000%
0.0440	100.000%
0.0380	100.000%
0.0040	100.000%
0.0030	100.000%
0.0010	0.000%
## Structure Detail:

## Structure #1 (Pond)

Sediment Basin 2

Pond Inputs:

Initial Pool Elev:	86.50 ft
Initial Pool:	0.46 ac-ft
*Sediment Storage:	0.00 ac-ft
Dead Space:	0.00 %

\*No sediment capacity defined

#### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	8.00	24.00	100.00	2.00	0.0150	93.50	2

## **Emergency Spillway**

Spillway Elev Crest Length (ft)		Left	Right	Bottom
		Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Spillway Elev Crest Length (ft)		Right Sideslope	Bottom Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Pond Results:

Peak Elevation:	93.43 ft
H'graph Detention Time:	15.10 hrs
Pond Model:	CSTRS
Dewater Time:	3.58 days
Trap Efficiency:	96.92 %

Dewatering time is calculated from peak stage to lowest spillway

## Elevation-Capacity-Discharge Table

Convright 1998 -2010 Pamela I. Schwah

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		Top of Sed. Storage
86.01	0.798	0.008	0.000		
86.50	1.061	0.462	0.000		
87.00	1.365	1.067	2.260	3.24*	
87.50	1.707	1.833	2.260	4.10*	
87.62	1.792	2.043	2.260	1.12*	
88.00	2.080	2.778	2.260	3.94*	
88.50	2.146	3.835	2.260	5.66*	
89.00	2.214	4.925	2.260	5.84*	
89.50	2.282	6.049	2.260	6.02*	
90.00	2.352	7.208	2.260	6.20*	
90.50	2.420	8.400	2.260	6.39*	
91.00	2.489	9.628	2.260	6.57*	
91.50	2.558	10.889	2.260	6.76*	
92.00	2.629	12.186	2.260	6.94*	
92.50	2.699	13.518	2.260	7.13*	
93.00	2.769	14.885	2.260	7.32*	
93.43	2.831	16.102	2.260	0.00	Peak Stage
93.50	2.841	16.287	2.260		Spillway #1
94.00	2.913	17.726	16.033		
94.50	2.986	19.200	41.216		
95.00	3.059	20.711	44.209		Spillway #2
95.50	3.134	22.260	57.188		
96.00	3.209	23.845	70.148		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

## **Detailed Discharge Table**

Elevation (ft)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
86.00	0.000	0.000	0.000	0.000	0.000
86.01	0.000	0.000	0.000	0.000	0.000
86.50	0.000	0.000	0.000	0.000	0.000
87.00	0.000	0.000	1.130	1.130	2.260
87.50	0.000	0.000	1.130	1.130	2.260
87.62	0.000	0.000	1.130	1.130	2.260
88.00	0.000	0.000	1.130	1.130	2.260
88.50	0.000	0.000	1.130	1.130	2.260
89.00	0.000	0.000	1.130	1.130	2.260
89.50	0.000	0.000	1.130	1.130	2.260

Elevation (ft)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
90.00	0.000	0.000	1.130	1.130	2.260
90.50	0.000	0.000	1.130	1.130	2.260
91.00	0.000	0.000	1.130	1.130	2.260
91.50	0.000	0.000	1.130	1.130	2.260
92.00	0.000	0.000	1.130	1.130	2.260
92.50	0.000	0.000	1.130	1.130	2.260
93.00	0.000	0.000	1.130	1.130	2.260
93.50	0.000	0.000	1.130	1.130	2.260
94.00	13.773	0.000	1.130	1.130	16.033
94.50	38.956	0.000	1.130	1.130	41.216
95.00	41.949	0.000	1.130	1.130	44.209
95.50	42.851	12.076	1.130	1.130	57.188
96.00	43.735	24.153	1.130	1.130	70.148

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	44.210	0.169	0.000	0.000	94.000	TR55	287.77	19.047
	Σ	44.210						287.77	19.047
#5	Σ	44.210						2.26	8.209

# Subwatershed Hydrology Detail:

# Subwatershed Sedimentology Detail:

Stru #	SWS #	Soil K	L (ft)	S (%)	С	Ρ	PS #	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc (ml/l)	24VW (ml/l)
#1	1	0.240	1,815.00	1.50	1.0000	1.0000	1	1,305.1	103,977	64.22	30.19
	Σ							1,305.1	103,977	64.22	30.19
#5	Σ							40.2	1,949,172	0.08	0.00

# Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.01	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169

# **Vulcan Orangeburg**

During Construction Sediment Basin 2 25-year, 24-hour storm event 7.1 inches

L.Lotrakul

# **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

## Particle Size Distribution:

Size (mm)	Coxville
1.4000	100.000%
1.0000	89.600%
0.0630	65.700%
0.0440	43.900%
0.0380	42.400%
0.0040	5.000%
0.0030	3.100%
0.0010	0.000%

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#5	4.810	0.162	Sediment Basin 2
Null	#5	==>	End	0.000	0.000	





# Structure Routing Details:

Stru #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	8. Large gullies, diversions, and low flowing streams	0.93	4.00	432.00	2.88	0.041
	1. Forest with heavy ground litter	0.08	1.00	1,202.00	0.07	4.769
#1	Muskingum K:					4.810

		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc. (ml/l)	24VW (ml/l)
#1	In	44 210	44 210	356.04	23.86	1,668.1	106,657	65.89	30.78
#1	Out	44.210	44.210	11.16	12.72	93.8	20,116	0.17	0.06
#5		0.000	44.210	10.97	12.72	93.8	2,152,965	18.28	0.06

# Structure Summary:

# Particle Size Distribution(s) at Each Structure

Size (mm)	In	Out
1.4000	100.000%	100.000%
1.0000	98.802%	100.000%
0.0630	72.448%	100.000%
0.0440	48.409%	100.000%
0.0380	46.755%	100.000%
0.0040	5.514%	98.003%
0.0030	3.418%	60.762%
0.0010	0.000%	0.000%

# Structure #1 (Sediment Basin 2 ):

Size (mm)	In/Out
1.4000	100.000%
1.0000	100.000%
0.0630	100.000%
0.0440	100.000%
0.0380	100.000%
0.0040	98.003%
0.0030	60.762%
0.0010	0.000%

## Structure Detail:

## Structure #1 (Pond)

Sediment Basin 2

Pond Inputs:

Initial Pool Elev:	86.50 ft
Initial Pool:	0.46 ac-ft
*Sediment Storage:	0.00 ac-ft
Dead Space:	0.00 %

\*No sediment capacity defined

#### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	8.00	24.00	100.00	2.00	0.0150	93.50	2

## **Emergency Spillway**

Spillway Elev	Crest Length Left		Right	Bottom
	(ft) Sideslope		Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev Crest Leng		Left	Right	Bottom
(ft)		Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Pond Results:

Peak Elevation:	93.82 ft
H'graph Detention Time:	11.17 hrs
Pond Model:	CSTRS
Dewater Time:	5.05 days
Trap Efficiency:	94.37 %

Dewatering time is calculated from peak stage to lowest spillway

## Elevation-Capacity-Discharge Table

Convright 1998 -2010 Pamela I. Schwah

Elevation	vation Area Capacity Discharge (ac) (ac-ft) (cfs)		Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		Top of Sed. Storage
86.01	0.798	0.008	0.000		
86.50	1.061	0.462	0.000		
87.00	1.365	1.067	2.260	3.24*	
87.50	1.707	1.833	2.260	4.10*	
87.62	1.792	2.043	2.260	1.12*	
88.00	2.080	2.778	2.260	3.94*	
88.50	2.146	3.835	2.260	5.66*	
89.00	2.214	4.925	2.260	5.84*	
89.50	2.282	6.049	2.260	6.02*	
90.00	2.352	7.208	2.260	6.20*	
90.50	2.420	8.400	2.260	6.39*	
91.00	2.489	9.628	2.260	6.57*	
91.50	2.558	10.889	2.260	6.76*	
92.00	2.629	12.186	2.260	6.94*	
92.50	2.699	13.518	2.260	7.13*	
93.00	2.769	14.885	2.260	7.32*	
93.50	2.841	16.287	2.260	7.51*	Spillway #1
93.82	2.888	17.216	11.158	35.50	Peak Stage
94.00	2.913	17.726	16.033		
94.50	2.986	19.200	41.216		
95.00	3.059	20.711	44.209		Spillway #2
95.50	3.134	22.260	57.188		
96.00	3.209	23.845	70.148		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

## **Detailed Discharge Table**

Elevation (ft)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
86.00	0.000	0.000	0.000	0.000	0.000
86.01	0.000	0.000	0.000	0.000	0.000
86.50	0.000	0.000	0.000	0.000	0.000
87.00	0.000	0.000	1.130	1.130	2.260
87.50	0.000	0.000	1.130	1.130	2.260
87.62	0.000	0.000	1.130	1.130	2.260
88.00	0.000	0.000	1.130	1.130	2.260
88.50	0.000	0.000	1.130	1.130	2.260
89.00	0.000	0.000	1.130	1.130	2.260
89.50	0.000	0.000	1.130	1.130	2.260

Elevation (ft)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
90.00	0.000	0.000	1.130	1.130	2.260
90.50	0.000	0.000	1.130	1.130	2.260
91.00	0.000	0.000	1.130	1.130	2.260
91.50	0.000	0.000	1.130	1.130	2.260
92.00	0.000	0.000	1.130	1.130	2.260
92.50	0.000	0.000	1.130	1.130	2.260
93.00	0.000	0.000	1.130	1.130	2.260
93.50	0.000	0.000	1.130	1.130	2.260
94.00	13.773	0.000	1.130	1.130	16.033
94.50	38.956	0.000	1.130	1.130	41.216
95.00	41.949	0.000	1.130	1.130	44.209
95.50	42.851	12.076	1.130	1.130	57.188
96.00	43.735	24.153	1.130	1.130	70.148

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	44.210	0.169	0.000	0.000	94.000	TR55	356.04	23.863
	Σ	44.210						356.04	23.863
#5	Σ	44.210						10.97	12.723

# Subwatershed Hydrology Detail:

# Subwatershed Sedimentology Detail:

Stru #	SWS #	Soil K	L (ft)	S (%)	С	Ρ	PS #	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc (ml/l)	24VW (ml/l)
#1	1	0.240	1,815.00	1.50	1.0000	1.0000	1	1,668.1	106,657	65.89	30.78
	Σ							1,668.1	106,657	65.89	30.78
#5	Σ							93.8	2,152,965	18.28	0.06

# Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.01	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169

# **Vulcan Orangeburg**

During Construction Sediment Basin 2 100-year, 24-hour storm event 9.3 inches

L.Lotrakul

# **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

## Particle Size Distribution:

Size (mm)	Coxville
1.4000	100.000%
1.0000	89.600%
0.0630	65.700%
0.0440	43.900%
0.0380	42.400%
0.0040	5.000%
0.0030	3.100%
0.0010	0.000%

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#5	4.810	0.162	Sediment Basin 2
Null	#5	==>	End	0.000	0.000	





# Structure Routing Details:

Stru #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	8. Large gullies, diversions, and low flowing streams	0.93	4.00	432.00	2.88	0.041
	1. Forest with heavy ground litter	0.08	1.00	1,202.00	0.07	4.769
#1	Muskingum K:					4.810

		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc. (ml/l)	24VW (ml/l)
#1	In	44 210	44 210	470.89	32.04	2,300.7	110,295	68.14	31.60
#1	Out	44.210	44.210	42.78	20.83	253.6	20,084	4.75	2.54
#5		0.000	44.210	40.45	20.83	253.6	2,301,353	543.98	2.45

# Structure Summary:

# Particle Size Distribution(s) at Each Structure

Size (mm)	In	Out
1.4000	100.000%	100.000%
1.0000	98.745%	100.000%
0.0630	72.406%	100.000%
0.0440	48.381%	100.000%
0.0380	46.728%	100.000%
0.0040	5.510%	49.992%
0.0030	3.416%	30.995%
0.0010	0.000%	0.000%

# Structure #1 (Sediment Basin 2 ):

|--|

Size (mm)	In/Out
1.4000	100.000%
1.0000	100.000%
0.0630	100.000%
0.0440	100.000%
0.0380	100.000%
0.0040	49.992%
0.0030	30.995%
0.0010	0.000%

## Structure Detail:

## Structure #1 (Pond)

Sediment Basin 2

Pond Inputs:

Initial Pool Elev:	86.50 ft
Initial Pool:	0.46 ac-ft
*Sediment Storage:	0.00 ac-ft
Dead Space:	0.00 %

\*No sediment capacity defined

#### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	8.00	24.00	100.00	2.00	0.0150	93.50	2

## **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

Pond Results:

Peak Elevation:	94.76 ft
H'graph Detention Time:	7.48 hrs
Pond Model:	CSTRS
Dewater Time:	3.68 days
Trap Efficiency:	88.98 %

Dewatering time is calculated from peak stage to lowest spillway

## Elevation-Capacity-Discharge Table

Convright 1998 -2010 Pamela I. Schwah

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		Top of Sed. Storage
86.01	0.798	0.008	0.000		
86.50	1.061	0.462	0.000		
87.00	1.365	1.067	2.260	3.24*	
87.50	1.707	1.833	2.260	4.10*	
87.62	1.792	2.043	2.260	1.12*	
88.00	2.080	2.778	2.260	3.94*	
88.50	2.146	3.835	2.260	5.66*	
89.00	2.214	4.925	2.260	5.84*	
89.50	2.282	6.049	2.260	6.02*	
90.00	2.352	7.208	2.260	6.20*	
90.50	2.420	8.400	2.260	6.39*	
91.00	2.489	9.628	2.260	6.57*	
91.50	2.558	10.889	2.260	6.76*	
92.00	2.629	12.186	2.260	6.94*	
92.50	2.699	13.518	2.260	7.13*	
93.00	2.769	14.885	2.260	7.32*	
93.50	2.841	16.287	2.260	7.51*	Spillway #1
94.00	2.913	17.726	16.033	1.09*	
94.50	2.986	19.200	41.216	1.85	
94.76	3.024	19.991	42.781	0.75	Peak Stage
95.00	3.059	20.711	44.209		Spillway #2
95.50	3.134	22.260	57.188		
96.00	3.209	23.845	70.148		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

## **Detailed Discharge Table**

Elevation (ft)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
86.00	0.000	0.000	0.000	0.000	0.000
86.01	0.000	0.000	0.000	0.000	0.000
86.50	0.000	0.000	0.000	0.000	0.000
87.00	0.000	0.000	1.130	1.130	2.260
87.50	0.000	0.000	1.130	1.130	2.260
87.62	0.000	0.000	1.130	1.130	2.260
88.00	0.000	0.000	1.130	1.130	2.260
88.50	0.000	0.000	1.130	1.130	2.260
89.00	0.000	0.000	1.130	1.130	2.260
89.50	0.000	0.000	1.130	1.130	2.260

Elevation (ft)	Enh. PerfRiser (cfs)	Emergency Spillway (cfs)	User- input discharge (cfs)	User- input discharge (cfs)	Combined Total Discharge (cfs)
90.00	0.000	0.000	1.130	1.130	2.260
90.50	0.000	0.000	1.130	1.130	2.260
91.00	0.000	0.000	1.130	1.130	2.260
91.50	0.000	0.000	1.130	1.130	2.260
92.00	0.000	0.000	1.130	1.130	2.260
92.50	0.000	0.000	1.130	1.130	2.260
93.00	0.000	0.000	1.130	1.130	2.260
93.50	0.000	0.000	1.130	1.130	2.260
94.00	13.773	0.000	1.130	1.130	16.033
94.50	38.956	0.000	1.130	1.130	41.216
95.00	41.949	0.000	1.130	1.130	44.209
95.50	42.851	12.076	1.130	1.130	57.188
96.00	43.735	24.153	1.130	1.130	70.148

Structure #5 (Null)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	44.210	0.169	0.000	0.000	94.000	TR55	470.89	32.037
	Σ	44.210						470.89	32.037
#5	Σ	44.210						40.45	20.832

# Subwatershed Hydrology Detail:

# Subwatershed Sedimentology Detail:

Stru #	SWS #	Soil K	L (ft)	S (%)	С	Ρ	PS #	Sediment (tons)	Peak Sediment Conc. (mg/l)	Peak Settleable Conc (ml/l)	24VW (ml/l)
#1	1	0.240	1,815.00	1.50	1.0000	1.0000	1	2,300.7	110,295	68.14	31.60
	Σ							2,300.7	110,295	68.14	31.60
#5	Σ							253.6	2,301,353	543.98	2.45

# Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.01	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 1 2-year, 24-hour Storm Event 3.8 inches* 

L.Lotrakul

## **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	2 yr - 24 hr
Rainfall Depth:	3.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#5	0.000	0.000	Detention Pond 1 (West)
Null	#3	==>	#5	0.000	0.000	Southwest Channel
Null	#5	==>	End	0.000	0.000	POI 1 (Wetlands, Stream, Existing, Shop, Office)





	Immediate Contributing Area (ac)		Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#3		1.990	1.990	5.10	0.36
#1	In	29,420	29 420	117.20	7.12
#1	Out	38.420	38.420	2.99	6.04
#5		235.720	276.130	31.00	42.98

# Structure Summary:

## Structure Detail:

#### Structure #3 (Null)

Southwest Channel

## Structure #1 (Pond)

Detention Pond 1 (West)

#### Pond Inputs:

			Initial Pool Elev:		89.50 ft		
			Initial Pool: (		0.68 ac-ft		
			Enhanced	Perf. Riser	<u>1</u>		
Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	4.50	24.00	75.00	1.30	0.0150	93.50	1

## **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	91.58 ft
Dewater Time:	3.14 days

Dewatering time is calculated from peak stage to lowest spillway

## Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		
89.25	1.348	0.304	0.000		
89.50	1.633	0.676	0.000		Low hole SPW #1
89.75	1.945	1.123	0.174	31.09*	
90.00	2.284	1.651	0.596	10.72*	
90.25	2.332	2.228	1.103	6.33*	
90.50	2.381	2.817	1.395	5.70	
90.75	2.430	3.419	1.636	4.85	
91.00	2.479	4.032	1.988	4.10	

Convright 1998 -2010 Pamela I. Schwah

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
91.25	2.530	4.658	2.514	3.35	
91.50	2.580	5.297	2.886	5.10	
91.58	2.598	5.518	2.992	4.10	Peak Stage
91.75	2.631	5.949	3.198		
92.00	2.683	6.613	3.476		
92.25	2.732	7.290	3.731		
92.50	2.782	7.979	3.968		
92.75	2.832	8.681	4.190		
93.00	2.882	9.395	4.400		
93.25	2.933	10.122	4.600		
93.50	2.984	10.861	4.792		Spillway #1
93.75	3.036	11.614	4.976		
94.00	3.088	12.379	13.773		
94.25	3.139	13.157	25.303		
94.50	3.190	13.948	33.171		
94.75	3.241	14.752	33.805		
95.00	3.293	15.569	34.428		Spillway #2
95.25	3.346	16.399	39.049		
95.50	3.398	17.242	43.660		
95.75	3.451	18.098	48.260		
96.00	3.505	18.968	60.966		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

## Detailed Discharge Table

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
89.00	0.000	0.000	0.000
89.25	0.000	0.000	0.000
89.50	8.00>0.000	0.000	0.000
89.75	0.174	0.000	0.174
90.00	0.596	0.000	0.596
90.25	1.103	0.000	1.103
90.50	1.395	0.000	1.395
90.75	6.00>1.636	0.000	1.636
91.00	1.988	0.000	1.988
91.25	2.514	0.000	2.514
91.50	2.886	0.000	2.886
91.75	3.198	0.000	3.198
92.00	3.476	0.000	3.476

Convright 1998 -2010 Pamela I. Schwah

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
92.25	3.731	0.000	3.731
92.50	3.968	0.000	3.968
92.75	4.190	0.000	4.190
93.00	4.400	0.000	4.400
93.25	4.600	0.000	4.600
93.50	4.792	0.000	4.792
93.75	4.976	0.000	4.976
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	33.171	0.000	33.171
94.75	33.805	0.000	33.805
95.00	34.428	0.000	34.428
95.25	35.040	4.010	39.049
95.50	35.641	8.019	43.660
95.75	36.232	12.029	48.260
96.00	36.813	24.153	60.966

## Structure #5 (Null)

POI 1 (Wetlands, Stream, Existing, Shop, Office)

Stru	SWS	SWS Area	Time of Conc	Musk K	Curve Musk X	Curve	UHS	Peak Discharge	Runoff Volume
#	#	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#3	1	1.990	0.285	0.027	0.283	84.000	TR55	5.10	0.362
	Σ	1.990						5.10	0.362
#1	1	38.420	0.171	0.027	0.283	84.000	TR55	117.20	7.119
	Σ	38.420						117.20	7.119
#5	1	235.720	16.953	0.000	0.000	80.000	TR55	28.18	36.577
	Σ	276.130						31.00	42.984

# Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171
#3	1	3. Short grass pasture	31.67	19.00	60.00	4.500	0.003
		8. Large gullies, diversions, and low flowing streams	0.26	4.00	1,548.00	1.520	0.282
#3	1	Time of Concentration:					0.285
#5	1	1. Forest with heavy ground litter	1.05	2.00	191.02	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,369.42	0.110	16.084
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.57	0.720	0.657
#5	1	Time of Concentration:					16.953

# Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#1	1	Muskingum K:					0.027
#3	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#3	1	Muskingum K:					0.027

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 1 10-year, 24-hour Storm Event 5.8 inches* 

L.Lotrakul

## **General Information**

# Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description			
Pond	#1	==>	#5	0.000	0.000	Detention Pond 1 (West)			
Null	#3	==>	#5	0.000	0.000	Southwest Channel			
Null	#5	==>	End	0.000	0.000	POI 1 (Wetlands, Stream, Existing, Shop, Office)			





		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#3		1.990	1.990	9.20	0.66
<i>щ</i> 1	In	20.420	20 420	210.64	13.00
#1	Out	38.420	38.420	4.55	10.61
#5		235.720	276.130	59.35	81.43

# Structure Summary:

## Structure Detail:

#### Structure #3 (Null)

Southwest Channel

### Structure #1 (Pond)

Detention Pond 1 (West)

#### Pond Inputs:

			Initial Pool Elev:		89.50 ft		
			Initial Pool: 0		0.68 ac-ft		
	Enhanced Perf. Riser						
Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	4.50	24.00	75.00	1.30	0.0150	93.50	1

## **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	93.19 ft
Dewater Time:	3.69 days

Dewatering time is calculated from peak stage to lowest spillway

## Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		
89.25	1.348	0.304	0.000		
89.50	1.633	0.676	0.000		Low hole SPW #1
89.75	1.945	1.123	0.174	31.09*	
90.00	2.284	1.651	0.596	10.72*	
90.25	2.332	2.228	1.103	6.33*	
90.50	2.381	2.817	1.395	5.11*	
90.75	2.430	3.419	1.636	4.45*	
91.00	2.479	4.032	1.988	4.15	

Convright 1998 -2010 Pamela I. Schwah

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
91.25	2.530	4.658	2.514	3.35	
91.50	2.580	5.297	2.886	2.90	
91.75	2.631	5.949	3.198	2.55	
92.00	2.683	6.613	3.476	2.45	
92.25	2.732	7.290	3.731	2.25	
92.50	2.782	7.979	3.968	2.15	
92.75	2.832	8.681	4.190	2.10	
93.00	2.882	9.395	4.400	3.15	
93.19	2.921	9.949	4.553	5.70	Peak Stage
93.25	2.933	10.122	4.600		
93.50	2.984	10.861	4.792		Spillway #1
93.75	3.036	11.614	4.976		
94.00	3.088	12.379	13.773		
94.25	3.139	13.157	25.303		
94.50	3.190	13.948	33.171		
94.75	3.241	14.752	33.805		
95.00	3.293	15.569	34.428		Spillway #2
95.25	3.346	16.399	39.049		
95.50	3.398	17.242	43.660		
95.75	3.451	18.098	48.260		
96.00	3.505	18.968	60.966		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

## Detailed Discharge Table

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
89.00	0.000	0.000	0.000
89.25	0.000	0.000	0.000
89.50	8.00>0.000	0.000	0.000
89.75	0.174	0.000	0.174
90.00	0.596	0.000	0.596
90.25	1.103	0.000	1.103
90.50	1.395	0.000	1.395
90.75	6.00>1.636	0.000	1.636
91.00	1.988	0.000	1.988
91.25	2.514	0.000	2.514
91.50	2.886	0.000	2.886
91.75	3.198	0.000	3.198
92.00	3.476	0.000	3.476
Convright 1998 -2010 Pamela I. Schwah

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
92.25	3.731	0.000	3.731
92.50	3.968	0.000	3.968
92.75	4.190	0.000	4.190
93.00	4.400	0.000	4.400
93.25	4.600	0.000	4.600
93.50	4.792	0.000	4.792
93.75	4.976	0.000	4.976
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	33.171	0.000	33.171
94.75	33.805	0.000	33.805
95.00	34.428	0.000	34.428
95.25	35.040	4.010	39.049
95.50	35.641	8.019	43.660
95.75	36.232	12.029	48.260
96.00	36.813	24.153	60.966

### Structure #5 (Null)

POI 1 (Wetlands, Stream, Existing, Shop, Office)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#3	1	1.990	0.285	0.027	0.283	84.000	TR55	9.20	0.662
	Σ	1.990						9.20	0.662
#1	1	38.420	0.171	0.027	0.283	84.000	TR55	210.64	12.999
	Σ	38.420						210.64	12.999
#5	1	235.720	16.953	0.000	0.000	80.000	TR55	54.81	70.156
	Σ	276.130						59.35	81.428

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171
#3	1	3. Short grass pasture	31.67	19.00	60.00	4.500	0.003
		8. Large gullies, diversions, and low flowing streams	0.26	4.00	1,548.00	1.520	0.282
#3	1	Time of Concentration:					0.285
#5	1	1. Forest with heavy ground litter	1.05	2.00	191.02	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,369.42	0.110	16.084
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.57	0.720	0.657
#5	1	Time of Concentration:					16.953

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#1	1	Muskingum K:					0.027
#3	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#3	1	Muskingum K:					0.027

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 1 25-year, 24-hour Storm Event 7.1 inches* 

L.Lotrakul

## **General Information**

## Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

<b>-</b>									
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description			
Pond	#1	==>	#5	0.000	0.000	Detention Pond 1 (West)			
Null	#3	==>	#5	0.000	0.000	Southwest Channel			
Null	#5	==>	End	0.000	0.000	POI 1 (Wetlands, Stream, Existing, Shop, Office)			





		Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
		(ac)	(ac)	(cfs)	(ac-ft)
#3		1.990	1.990	11.89	0.86
#1	In	29 420	29 420	271.80	16.97
#1	Out	50.420	50.420	10.89	13.92
#5		235.720	276.130	78.21	108.03

## Structure Summary:

### Structure Detail:

### Structure #3 (Null)

Southwest Channel

### Structure #1 (Pond)

Detention Pond 1 (West)

### Pond Inputs:

			Initial Pool Elev:		89.50 ft		
			Initial Pool: 0.68 ac-ft		0.68 ac-ft		
			Enhanced	Perf. Riser	<u></u>		
Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	4.50	24.00	75.00	1.30	0.0150	93.50	1

### Emergency Spillway

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

### Pond Results:

Peal	K Elevation:	93.92 ft
Dev	vater Time:	3.98 days

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		
89.25	1.348	0.304	0.000		
89.50	1.633	0.676	0.000		Low hole SPW #1
89.75	1.945	1.123	0.174	31.09*	
90.00	2.284	1.651	0.596	10.72*	
90.25	2.332	2.228	1.103	6.33*	
90.50	2.381	2.817	1.395	5.11*	
90.75	2.430	3.419	1.636	4.45*	
91.00	2.479	4.032	1.988	3.74*	

Convright 1998 -2010 Pamela I. Schwah

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
91.25	2.530	4.658	2.514	3.40	
91.50	2.580	5.297	2.886	2.85	
91.75	2.631	5.949	3.198	2.60	
92.00	2.683	6.613	3.476	2.40	
92.25	2.732	7.290	3.731	2.25	
92.50	2.782	7.979	3.968	2.20	
92.75	2.832	8.681	4.190	2.05	
93.00	2.882	9.395	4.400	2.05	
93.25	2.933	10.122	4.600	1.95	
93.50	2.984	10.861	4.792	1.90	Spillway #1
93.75	3.036	11.614	4.976	5.35	
93.92	3.071	12.128	10.891	5.15	Peak Stage
94.00	3.088	12.379	13.773		
94.25	3.139	13.157	25.303		
94.50	3.190	13.948	33.171		
94.75	3.241	14.752	33.805		
95.00	3.293	15.569	34.428		Spillway #2
95.25	3.346	16.399	39.049		
95.50	3.398	17.242	43.660		
95.75	3.451	18.098	48.260		
96.00	3.505	18.968	60.966		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

### Detailed Discharge Table

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
89.00	0.000	0.000	0.000
89.25	0.000	0.000	0.000
89.50	8.00>0.000	0.000	0.000
89.75	0.174	0.000	0.174
90.00	0.596	0.000	0.596
90.25	1.103	0.000	1.103
90.50	1.395	0.000	1.395
90.75	6.00>1.636	0.000	1.636
91.00	1.988	0.000	1.988
91.25	2.514	0.000	2.514
91.50	2.886	0.000	2.886
91.75	3.198	0.000	3.198
92.00	3.476	0.000	3.476

Convright 1998 -2010 Pamela I. Schwah

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
92.25	3.731	0.000	3.731
92.50	3.968	0.000	3.968
92.75	4.190	0.000	4.190
93.00	4.400	0.000	4.400
93.25	4.600	0.000	4.600
93.50	4.792	0.000	4.792
93.75	4.976	0.000	4.976
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	33.171	0.000	33.171
94.75	33.805	0.000	33.805
95.00	34.428	0.000	34.428
95.25	35.040	4.010	39.049
95.50	35.641	8.019	43.660
95.75	36.232	12.029	48.260
96.00	36.813	24.153	60.966

### Structure #5 (Null)

POI 1 (Wetlands, Stream, Existing, Shop, Office)

Stru #	SWS #	SWS Area (ac)	Time of Conc (brs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge	Runoff Volume (ac-ft)
#3	1	1.990	0.285	0.027	0.283	84.000	TR55	11.89	0.864
	Σ	1.990						11.89	0.864
#1	1	38.420	0.171	0.027	0.283	84.000	TR55	271.80	16.972
	Σ	38.420						271.80	16.972
#5	1	235.720	16.953	0.000	0.000	80.000	TR55	73.17	93.252
	Σ	276.130						78.21	108.032

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171
#3	1	3. Short grass pasture	31.67	19.00	60.00	4.500	0.003
		8. Large gullies, diversions, and low flowing streams	0.26	4.00	1,548.00	1.520	0.282
#3	1	Time of Concentration:					0.285
#5	1	1. Forest with heavy ground litter	1.05	2.00	191.02	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,369.42	0.110	16.084
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.57	0.720	0.657
#5	1	Time of Concentration:					16.953

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#1	1	Muskingum K:					0.027
#3	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#3	1	Muskingum K:					0.027

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 1 100-year, 24-hour Storm Event 9.3 inches* 

L.Lotrakul

## **General Information**

## Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description	
Pond	#1	==>	#5	0.000	0.000	Detention Pond 1 (West)	
Null	#3	==>	#5	0.000	0.000	Southwest Channel	
Null	#5	==>	End	0.000	0.000	POI 1 (Wetlands, Stream, Existing, Shop, Office)	





	Immediate Contributing Area (ac)		Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#3		1.990	1.990	16.43	1.21
#1	In	29 420	29 420	374.87	23.83
<sup>#1</sup>	Out	38.420	38.420	33.87	20.59
#5		235.720	276.130	110.27	155.31

## Structure Summary:

### Structure Detail:

### Structure #3 (Null)

Southwest Channel

#### Structure #1 (Pond)

Detention Pond 1 (West)

### Pond Inputs:

Initial Pool Elev:	89.50 ft				
Initial Pool:	0.68 ac-ft				
Enhanced Perf. Riser					

#### Riser Barrel Number of Riser Height Barrel Slope Spillway Elev Barrel Diameter Diameter Manning's n Holes per (ft) Length (ft) (ft) (%) (in) (in) Elev 75.00 48.00 4.50 24.00 93.50 1 1.30 0.0150

### Emergency Spillway

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

### Pond Results:

Peak Elevation:	94.78 ft
Dewater Time:	4.08 days

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
89.00	1.091	0.000	0.000		
89.25	1.348	0.304	0.000		
89.50	1.633	0.676	0.000		Low hole SPW #1
89.75	1.945	1.123	0.174	31.09*	
90.00	2.284	1.651	0.596	10.72*	
90.25	2.332	2.228	1.103	6.33*	
90.50	2.381	2.817	1.395	5.11*	
90.75	2.430	3.419	1.636	4.45*	
91.00	2.479	4.032	1.988	3.74*	

Convright 1998 -2010 Pamela I. Schwah

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
91.25	2.530	4.658	2.514	3.40	
91.50	2.580	5.297	2.886	2.85	
91.75	2.631	5.949	3.198	2.60	
92.00	2.683	6.613	3.476	2.45	
92.25	2.732	7.290	3.731	2.25	
92.50	2.782	7.979	3.968	2.15	
92.75	2.832	8.681	4.190	2.10	
93.00	2.882	9.395	4.400	2.00	
93.25	2.933	10.122	4.600	1.95	
93.50	2.984	10.861	4.792	1.90	Spillway #1
93.75	3.036	11.614	4.976	4.40	
94.00	3.088	12.379	13.773	5.55	
94.25	3.139	13.157	25.303	1.30	
94.50	3.190	13.948	33.171	0.65	
94.75	3.241	14.752	33.805	0.80	
94.78	3.247	14.842	33.874	0.20	Peak Stage
95.00	3.293	15.569	34.428		Spillway #2
95.25	3.346	16.399	39.049		
95.50	3.398	17.242	43.660		
95.75	3.451	18.098	48.260		
96.00	3.505	18.968	60.966		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

### Detailed Discharge Table

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
89.00	0.000	0.000	0.000
89.25	0.000	0.000	0.000
89.50	8.00>0.000	0.000	0.000
89.75	0.174	0.000	0.174
90.00	0.596	0.000	0.596
90.25	1.103	0.000	1.103
90.50	1.395	0.000	1.395
90.75	6.00>1.636	0.000	1.636
91.00	1.988	0.000	1.988
91.25	2.514	0.000	2.514
91.50	2.886	0.000	2.886
91.75	3.198	0.000	3.198
92.00	3.476	0.000	3.476

Convright 1998 -2010 Pamela I. Schwah

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
92.25	3.731	0.000	3.731
92.50	3.968	0.000	3.968
92.75	4.190	0.000	4.190
93.00	4.400	0.000	4.400
93.25	4.600	0.000	4.600
93.50	4.792	0.000	4.792
93.75	4.976	0.000	4.976
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	33.171	0.000	33.171
94.75	33.805	0.000	33.805
95.00	34.428	0.000	34.428
95.25	35.040	4.010	39.049
95.50	35.641	8.019	43.660
95.75	36.232	12.029	48.260
96.00	36.813	24.153	60.966

### Structure #5 (Null)

POI 1 (Wetlands, Stream, Existing, Shop, Office)

Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#3	1	1.990	0.285	0.027	0.283	84.000	TR55	16.43	1.213
	Σ	1.990						16.43	1.213
#1	1	38.420	0.171	0.027	0.283	84.000	TR55	374.87	23.827
	Σ	38.420						374.87	23.827
#5	1	235.720	16.953	0.000	0.000	80.000	TR55	105.12	133.505
	Σ	276.130						110.27	155.308

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	32.31	21.00	65.00	2.840	0.006
		8. Large gullies, diversions, and low flowing streams	0.94	16.00	1,703.03	2.900	0.163
		8. Large gullies, diversions, and low flowing streams	20.00	27.00	135.00	13.410	0.002
#1	1	Time of Concentration:					0.171
#3	1	3. Short grass pasture	31.67	19.00	60.00	4.500	0.003
		8. Large gullies, diversions, and low flowing streams	0.26	4.00	1,548.00	1.520	0.282
#3	1	Time of Concentration:					0.285
#5	1	1. Forest with heavy ground litter	1.05	2.00	191.02	0.250	0.212
		4. Cultivated, straight row	0.02	1.00	6,369.42	0.110	16.084
		8. Large gullies, diversions, and low flowing streams	0.06	1.00	1,703.57	0.720	0.657
#5	1	Time of Concentration:					16.953

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#1	1	Muskingum K:					0.027
#3	1	3. Short grass pasture	3.33	3.00	90.00	1.460	0.017
		8. Large gullies, diversions, and low flowing streams	0.89	1.00	112.00	2.830	0.010
#3	1	Muskingum K:					0.027

## **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 2 2-year, 24-hour Storm Event 3.8 inches* 

L.Lotrakul

## **General Information**

## Storm Information:

Storm Type:	NRCS Type II
Design Storm:	2 yr - 24 hr
Rainfall Depth:	3.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#4	0.000	0.000	Detention Pond 2 (East)
Null	#3	==>	#4	0.000	0.000	Southeast Channel
Null	#4	==>	End	0.000	0.000	POI 2 (includes Western Portion of Wetlands)

## Structure Networking:



		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#3		2.520	2.520	6.08	0.45
#1	In	44 210	44 210	135.29	8.20
#1	Out	44.210	44.210	3.58	7.42
#4		13.440	60.170	15.28	9.88

## Structure Summary:

### Structure Detail:

### Structure #3 (Null)

Southeast Channel

#### Structure #1 (Pond)

Detention Pond 2 (East)

### Pond Inputs:

Initial Pool Elev:	86.50 ft
Initial Pool:	0.46 ac-ft

### Enhanced Perf. Riser

Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	7.50	24.00	100.00	2.00	0.0150	93.50	1

### **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

### Pond Results:

Peak Elevation:	89.46 ft
Dewater Time:	2.57 days

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		
86.25	0.921	0.214	0.000		
86.50	1.058	0.461	0.000		Low hole SPW #1
86.75	1.204	0.744	0.174	19.66*	
87.00	1.360	1.064	0.596	6.50*	
87.25	1.526	1.425	1.103	3.96*	
87.50	1.701	1.828	1.395	3.95	
87.75	1.886	2.276	1.636	3.60	
88.00	2.080	2.772	1.846	3.45	

Convright 1998 -2010 Pamela I Schwah

Elevation	Area	Capacity	Discharge	Dewater Time	
Lievation	(ac)	(ac-ft)	(cfs)	(hrs)	
88.25	2.113	3.296	2.034	3.25	
88.50	2.146	3.828	2.206	3.05	
88.75	2.180	4.369	2.508	2.80	
89.00	2.214	4.918	2.996	2.40	
89.25	2.248	5.476	3.336	3.45	
89.46	2.277	5.960	3.581	5.65	Peak Stage
89.50	2.282	6.042	3.623		
89.75	2.317	6.617	3.879		
90.00	2.352	7.201	4.115		
90.25	2.386	7.793	4.336		
90.50	2.420	8.394	4.544		
90.75	2.454	9.003	4.741		
91.00	2.489	9.621	4.930		
91.25	2.523	10.247	5.111		
91.50	2.558	10.882	5.285		
91.75	2.594	11.526	5.454		
92.00	2.629	12.179	5.617		
92.25	2.664	12.841	5.775		
92.50	2.699	13.511	5.929		
92.75	2.734	14.190	6.079		
93.00	2.769	14.878	6.225		
93.25	2.805	15.575	6.367		
93.50	2.841	16.280	6.507		Spillway #1
93.75	2.877	16.995	6.643		
94.00	2.913	17.719	13.773		
94.25	2.949	18.452	25.303		
94.50	2.986	19.193	38.956		
94.75	3.022	19.944	40.558		
95.00	3.059	20.705	41.027		Spillway #2
95.25	3.096	21.474	45.500		
95.50	3.134	22.253	49.968		
95.75	3.171	23.041	54.431		
96.00	3.209	23.838	67.004		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

Detailed Discharge Table

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
86.00	0.000	0.000	0.000
86.25	0.000	0.000	0.000
86.50	8.00>0.000	0.000	0.000
86.75	0.174	0.000	0.174
87.00	0.596	0.000	0.596
87.25	1.103	0.000	1.103
87.50	1.395	0.000	1.395
87.75	1.636	0.000	1.636
88.00	1.846	0.000	1.846
88.25	2.034	0.000	2.034
88.50	6.00>2.206	0.000	2.206
88.75	2.508	0.000	2.508
89.00	2.996	0.000	2.996
89.25	3.336	0.000	3.336
89.50	3.623	0.000	3.623
89.75	3.879	0.000	3.879
90.00	4.115	0.000	4.115
90.25	4.336	0.000	4.336
90.50	4.544	0.000	4.544
90.75	4.741	0.000	4.741
91.00	4.930	0.000	4.930
91.25	5.111	0.000	5.111
91.50	5.285	0.000	5.285
91.75	5.454	0.000	5.454
92.00	5.617	0.000	5.617
92.25	5.775	0.000	5.775
92.50	5.929	0.000	5.929
92.75	6.079	0.000	6.079
93.00	6.225	0.000	6.225
93.25	6.367	0.000	6.367
93.50	6.507	0.000	6.507
93.75	6.643	0.000	6.643
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	38.956	0.000	38.956
94.75	40.558	0.000	40.558
95.00	41.027	0.000	41.027
95.25	41.491	4.010	45.500
95.50	41.949	8.019	49.968
95.75	42.403	12.029	54.431
96.00	42.851	24.153	67.004

<u>Structure #4 (Null)</u>

POI 2 (includes Western Portion of Wetlands)

Stru	SWS	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
π	π	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#3	1	2.520	0.324	0.003	0.254	84.000	TR55	6.08	0.453
	Σ	2.520						6.08	0.453
#1	1	44.210	0.169	0.000	0.000	84.000	TR55	135.29	8.203
	Σ	44.210						135.29	8.203
#4	1	13.440	1.210	0.331	0.126	79.000	TR55	11.81	2.000
	Σ	60.170						15.28	9.876

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.00	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169
#3	1	3. Short grass pasture	33.33	19.00	57.00	4.610	0.003
		8. Large gullies, diversions, and low flowing streams	0.35	7.20	2,046.03	1.770	0.321
#3	1	Time of Concentration:					0.324
#4	1	1. Forest with heavy ground litter	0.19	0.30	154.00	0.110	0.388
		4. Cultivated, straight row	0.08	0.50	656.00	0.240	0.759
		8. Large gullies, diversions, and low flowing streams	0.22	0.70	319.00	1.400	0.063
#4	1	Time of Concentration:					1.210

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#3	1	6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#3	1	Muskingum K:					0.003
#4	1	8. Large gullies, diversions, and low flowing streams	0.03	0.20	627.00	0.530	0.328
		6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#4	1	Muskingum K:					0.331

## **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 2 10-year, 24-hour Storm Event 5.8 inches* 

L.Lotrakul

## **General Information**

## Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#4	0.000	0.000	Detention Pond 2 (East)
Null	#3	==>	#4	0.000	0.000	Southeast Channel
Null	#4	==>	End	0.000	0.000	POI 2 (includes Western Portion of Wetlands)

## Structure Networking:



		Immediate Contributing Area	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#3		2.520	2.520	10.99	0.83
#1	In	44 210	44 210	243.14	14.98
#1	Out	44.210	44.210	5.32	12.54
#4		13.440	60.170	28.47	17.25

## Structure Summary:

### Structure Detail:

### Structure #3 (Null)

Southeast Channel

### Structure #1 (Pond)

Detention Pond 2 (East)

### Pond Inputs:

			Initial Pool	Elev:	86.50 ft		
			Initial	Pool:	0.46 ac-ft		
			Enhanced	Perf. Riser	<u>1</u>		
Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	7.50	24.00	100.00	2.00	0.0150	93.50	1

### **Emergency Spillway**

Spillway Elev	Crest Length	Left	Right	Bottom
	(ft)	Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	91.56 ft
Dewater Time:	3.10 days

Dewatering time is calculated from peak stage to lowest spillway

### Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		
86.25	0.921	0.214	0.000		
86.50	1.058	0.461	0.000		Low hole SPW #1
86.75	1.204	0.744	0.174	19.66*	
87.00	1.360	1.064	0.596	6.50*	
87.25	1.526	1.425	1.103	3.96*	
87.50	1.701	1.828	1.395	3.50*	
87.75	1.886	2.276	1.636	3.31*	
88.00	2.080	2.772	1.846	3.25*	

5

Convright 1998 -2010 Pamela I Schwah

Elevation	Area	Capacity	Discharge	Dewater Time	
	(ac)	(ac-ft)	(cfs)	(hrs)	
88.25	2.113	3.296	2.034	3.12*	
88.50	2.146	3.828	2.206	3.05	
88.75	2.180	4.369	2.508	2.80	
89.00	2.214	4.918	2.996	2.40	
89.25	2.248	5.476	3.336	2.15	
89.50	2.282	6.042	3.623	1.95	
89.75	2.317	6.617	3.879	1.85	
90.00	2.352	7.201	4.115	1.80	
90.25	2.386	7.793	4.336	1.70	
90.50	2.420	8.394	4.544	1.65	
90.75	2.454	9.003	4.741	1.55	
91.00	2.489	9.621	4.930	1.55	
91.25	2.523	10.247	5.111	2.30	
91.50	2.558	10.882	5.285	3.75	
91.56	2.567	11.032	5.324	2.55	Peak Stage
91.75	2.594	11.526	5.454		
92.00	2.629	12.179	5.617		
92.25	2.664	12.841	5.775		
92.50	2.699	13.511	5.929		
92.75	2.734	14.190	6.079		
93.00	2.769	14.878	6.225		
93.25	2.805	15.575	6.367		
93.50	2.841	16.280	6.507		Spillway #1
93.75	2.877	16.995	6.643		
94.00	2.913	17.719	13.773		
94.25	2.949	18.452	25.303		
94.50	2.986	19.193	38.956		
94.75	3.022	19.944	40.558		
95.00	3.059	20.705	41.027		Spillway #2
95.25	3.096	21.474	45.500		
95.50	3.134	22.253	49.968		
95.75	3.171	23.041	54.431		
96.00	3.209	23.838	67.004		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

Detailed Discharge Table

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
86.00	0.000	0.000	0.000
86.25	0.000	0.000	0.000
86.50	8.00>0.000	0.000	0.000
86.75	0.174	0.000	0.174
87.00	0.596	0.000	0.596
87.25	1.103	0.000	1.103
87.50	1.395	0.000	1.395
87.75	1.636	0.000	1.636
88.00	1.846	0.000	1.846
88.25	2.034	0.000	2.034
88.50	6.00>2.206	0.000	2.206
88.75	2.508	0.000	2.508
89.00	2.996	0.000	2.996
89.25	3.336	0.000	3.336
89.50	3.623	0.000	3.623
89.75	3.879	0.000	3.879
90.00	4.115	0.000	4.115
90.25	4.336	0.000	4.336
90.50	4.544	0.000	4.544
90.75	4.741	0.000	4.741
91.00	4.930	0.000	4.930
91.25	5.111	0.000	5.111
91.50	5.285	0.000	5.285
91.75	5.454	0.000	5.454
92.00	5.617	0.000	5.617
92.25	5.775	0.000	5.775
92.50	5.929	0.000	5.929
92.75	6.079	0.000	6.079
93.00	6.225	0.000	6.225
93.25	6.367	0.000	6.367
93.50	6.507	0.000	6.507
93.75	6.643	0.000	6.643
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	38.956	0.000	38.956
94.75	40.558	0.000	40.558
95.00	41.027	0.000	41.027
95.25	41.491	4.010	45.500
95.50	41.949	8.019	49.968
95.75	42.403	12.029	54.431
96.00	42.851	24.153	67.004

<u>Structure #4 (Null)</u>

POI 2 (includes Western Portion of Wetlands)

Stru	SWS	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
#	#	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#3	1	2.520	0.324	0.003	0.254	84.000	TR55	10.99	0.828
	Σ	2.520						10.99	0.828
#1	1	44.210	0.169	0.000	0.000	84.000	TR55	243.14	14.979
	Σ	44.210						243.14	14.979
#4	1	13.440	1.210	0.331	0.126	79.000	TR55	23.29	3.886
	Σ	60.170						28.47	17.254

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.00	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169
#3	1	3. Short grass pasture	33.33	19.00	57.00	4.610	0.003
		8. Large gullies, diversions, and low flowing streams	0.35	7.20	2,046.03	1.770	0.321
#3	1	Time of Concentration:					0.324
#4	1	1. Forest with heavy ground litter	0.19	0.30	154.00	0.110	0.388
		4. Cultivated, straight row	0.08	0.50	656.00	0.240	0.759
		8. Large gullies, diversions, and low flowing streams	0.22	0.70	319.00	1.400	0.063
#4	1	Time of Concentration:					1.210

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#3	1	6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#3	1	Muskingum K:					0.003
#4	1	8. Large gullies, diversions, and low flowing streams	0.03	0.20	627.00	0.530	0.328
		6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#4	1	Muskingum K:					0.331
## **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 2 25-year, 24-hour Storm Event 7.1 inches* 

L.Lotrakul

#### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#4	0.000	0.000	Detention Pond 2 (East)
Null	#3	==>	#4	0.000	0.000	Southeast Channel
Null	#4	==>	End	0.000	0.000	POI 2 (includes Western Portion of Wetlands)

## Structure Networking:



		Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#3		2.520	2.520	14.21	1.08
	In	2.520	2.520	313.74	19.56
#1	Out	44.210	44.210	6.17	15.72
#4		13.440	60.170	37.06	22.00

#### Structure Summary:

#### Structure Detail:

#### Structure #3 (Null)

Southeast Channel

#### Structure #1 (Pond)

Detention Pond 2 (East)

#### Pond Inputs:

			Initial Pool Elev: 86				
			Initial Pool: 0.46 ac-ft				
			Enhanced	Perf. Riser	<u>.</u>		
Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	7.50	24.00	100.00	2.00	0.0150	93.50	1

#### Emergency Spillway

Spillway Elev Crest Length (ft)		Left	Right	Bottom
		Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	92.91 ft
Dewater Time:	3.39 days

Dewatering time is calculated from peak stage to lowest spillway

#### Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		
86.25	0.921	0.214	0.000		
86.50	1.058	0.461	0.000		Low hole SPW #1
86.75	1.204	0.744	0.174	19.66*	
87.00	1.360	1.064	0.596	6.50*	
87.25	1.526	1.425	1.103	3.96*	
87.50	1.701	1.828	1.395	3.50*	
87.75	1.886	2.276	1.636	3.31*	
88.00	2.080	2.772	1.846	3.25*	

#### **SEDCAD 4 for Windows**

Convright 1998 -2010 Pamela I Schwah

Elevation	Area	Capacity	Discharge	Dewater Time	
	(ac)	(ac-ft)	(cfs)	(hrs)	
88.25	2.113	3.296	2.034	3.12*	
88.50	2.146	3.828	2.206	2.92*	
88.75	2.180	4.369	2.508	2.61*	
89.00	2.214	4.918	2.996	2.40	
89.25	2.248	5.476	3.336	2.15	
89.50	2.282	6.042	3.623	2.00	
89.75	2.317	6.617	3.879	1.85	
90.00	2.352	7.201	4.115	1.75	
90.25	2.386	7.793	4.336	1.70	
90.50	2.420	8.394	4.544	1.65	
90.75	2.454	9.003	4.741	1.55	
91.00	2.489	9.621	4.930	1.55	
91.25	2.523	10.247	5.111	1.55	
91.50	2.558	10.882	5.285	1.45	
91.75	2.594	11.526	5.454	1.45	
92.00	2.629	12.179	5.617	1.45	
92.25	2.664	12.841	5.775	1.40	
92.50	2.699	13.511	5.929	1.40	
92.75	2.734	14.190	6.079	3.20	
92.91	2.756	14.619	6.170	3.95	Peak Stage
93.00	2.769	14.878	6.225		
93.25	2.805	15.575	6.367		
93.50	2.841	16.280	6.507		Spillway #1
93.75	2.877	16.995	6.643		
94.00	2.913	17.719	13.773		
94.25	2.949	18.452	25.303		
94.50	2.986	19.193	38.956		
94.75	3.022	19.944	40.558		
95.00	3.059	20.705	41.027		Spillway #2
95.25	3.096	21.474	45.500		
95.50	3.134	22.253	49.968		
95.75	3.171	23.041	54.431		
96.00	3.209	23.838	67.004		

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

Detailed Discharge Table

## SEDCAD 4 for Windows

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
86.00	0.000	0.000	0.000
86.25	0.000	0.000	0.000
86.50	8.00>0.000	0.000	0.000
86.75	0.174	0.000	0.174
87.00	0.596	0.000	0.596
87.25	1.103	0.000	1.103
87.50	1.395	0.000	1.395
87.75	1.636	0.000	1.636
88.00	1.846	0.000	1.846
88.25	2.034	0.000	2.034
88.50	6.00>2.206	0.000	2.206
88.75	2.508	0.000	2.508
89.00	2.996	0.000	2.996
89.25	3.336	0.000	3.336
89.50	3.623	0.000	3.623
89.75	3.879	0.000	3.879
90.00	4.115	0.000	4.115
90.25	4.336	0.000	4.336
90.50	4.544	0.000	4.544
90.75	4.741	0.000	4.741
91.00	4.930	0.000	4.930
91.25	5.111	0.000	5.111
91.50	5.285	0.000	5.285
91.75	5.454	0.000	5.454
92.00	5.617	0.000	5.617
92.25	5.775	0.000	5.775
92.50	5.929	0.000	5.929
92.75	6.079	0.000	6.079
93.00	6.225	0.000	6.225
93.25	6.367	0.000	6.367
93.50	6.507	0.000	6.507
93.75	6.643	0.000	6.643
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	38.956	0.000	38.956
94.75	40.558	0.000	40.558
95.00	41.027	0.000	41.027
95.25	41.491	4.010	45.500
95.50	41.949	8.019	49.968
95.75	42.403	12.029	54.431
96.00	42.851	24.153	67.004

<u>Structure #4 (Null)</u>

POI 2 (includes Western Portion of Wetlands)

Stru	SWS	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
#	#	(ac)	(hrs)	(hrs)		Number		(cfs)	(ac-ft)
#3	1	2.520	0.324	0.003	0.254	84.000	TR55	14.21	1.082
	Σ	2.520						14.21	1.082
#1	1	44.210	0.169	0.000	0.000	84.000	TR55	313.74	19.557
	Σ	44.210						313.74	19.557
#4	1	13.440	1.210	0.331	0.126	79.000	TR55	31.11	5.189
	Σ	60.170						37.06	21.995

### Subwatershed Hydrology Detail:

#### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.00	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169
#3	1	3. Short grass pasture	33.33	19.00	57.00	4.610	0.003
		8. Large gullies, diversions, and low flowing streams	0.35	7.20	2,046.03	1.770	0.321
#3	1	Time of Concentration:					0.324
#4	1	1. Forest with heavy ground litter	0.19	0.30	154.00	0.110	0.388
		4. Cultivated, straight row	0.08	0.50	656.00	0.240	0.759
		8. Large gullies, diversions, and low flowing streams	0.22	0.70	319.00	1.400	0.063
#4	1	Time of Concentration:					1.210

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#3	1	6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#3	1	Muskingum K:					0.003
#4	1	8. Large gullies, diversions, and low flowing streams	0.03	0.20	627.00	0.530	0.328
		6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#4	1	Muskingum K:					0.331

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 2 100-year, 24-hour Storm Event 9.3 inches* 

L.Lotrakul

1

#### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description
Pond	#1	==>	#4	0.000	0.000	Detention Pond 2 (East)
Null	#3	==>	#4	0.000	0.000	Southeast Channel
Null	#4	==>	End	0.000	0.000	POI 2 (includes Western Portion of Wetlands)

## Structure Networking:



		Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
		(ac)	(ac)	(cfs)	(ac-ft)
#3	}	2.520	2.520	19.65	1.52
#1	In	44 210	44 210	432.70	27.46
#1	Out	44.210	44.210	23.18	22.27
#4	ŀ	13.440	60.170	67.07	31.25

#### Structure Summary:

#### Structure Detail:

#### Structure #3 (Null)

Southeast Channel

#### Structure #1 (Pond)

Detention Pond 2 (East)

#### Pond Inputs:

			Initial Pool Elev: 86.50		86.50 ft		
			Initial Pool: 0.46 ac-ft		0.46 ac-ft		
			Enhanced	Perf. Riser	-		
Riser Diameter (in)	Riser Height (ft)	Barrel Diameter (in)	Barrel Length (ft)	Barrel Slope (%)	Manning's n	Spillway Elev (ft)	Number of Holes per Elev
48.00	7.50	24.00	100.00	2.00	0.0150	93.50	1

#### Emergency Spillway

Spillway Elev Crest Length (ft)		Left	Right	Bottom
		Sideslope	Sideslope	Width (ft)
95.00	30.00	3.00:1	3.00:1	10.00

#### Pond Results:

Peak Elevation:	94.20 ft
Dewater Time:	3.76 days

Dewatering time is calculated from peak stage to lowest spillway

#### Elevation-Capacity-Discharge Table

Elevation	Area (ac)	Capacity (ac-ft)	Discharge (cfs)	Dewater Time (hrs)	
86.00	0.793	0.000	0.000		
86.25	0.921	0.214	0.000		
86.50	1.058	0.461	0.000		Low hole SPW #1
86.75	1.204	0.744	0.174	19.66*	
87.00	1.360	1.064	0.596	6.50*	
87.25	1.526	1.425	1.103	3.96*	
87.50	1.701	1.828	1.395	3.50*	
87.75	1.886	2.276	1.636	3.31*	
88.00	2.080	2.772	1.846	3.25*	

#### **SEDCAD 4 for Windows**

Convright 1998 -2010 Pamela I Schwah

Flouration	Area	Capacity	Discharge	Dewater Time		
Elevation	(ac)	(ac-ft)	(cfs)	(hrs)		
88.25	2.113	3.296	2.034	3.12*		
88.50	2.146	3.828	2.206	2.92*		
88.75	2.180	4.369	2.508	2.61*		
89.00	2.214	4.918	2.996	2.22*		
89.25	2.248	5.476	3.336	2.02*		
89.50	2.282	6.042	3.623	1.89*		
89.75	2.317	6.617	3.879	1.85		
90.00	2.352	7.201	4.115	1.75		
90.25	2.386	7.793	4.336	1.70		
90.50	2.420	8.394	4.544	1.65		
90.75	2.454	9.003	4.741	1.55		
91.00	2.489	9.621	4.930	1.55		
91.25	2.523	10.247	5.111	1.55		
91.50	2.558	10.882	5.285	1.45		
91.75	2.594	11.526	5.454	1.45		
92.00	2.629	12.179	5.617	1.45		
92.25	2.664	12.841	5.775	1.40		
92.50	2.699	13.511	5.929	1.40		
92.75	2.734	14.190	6.079	1.35		
93.00	2.769	14.878	6.225	1.35		
93.25	2.805	15.575	6.367	1.35		
93.50	2.841	16.280	6.507	1.30	Spillway #1	
93.75	2.877	16.995	6.643	4.35		
94.00	2.913	17.719	13.773	4.60		
94.20	2.943	18.317	23.183	2.15	Peak Stage	
94.25	2.949	18.452	25.303			
94.50	2.986	19.193	38.956			
94.75	3.022	19.944	40.558			
95.00	3.059	20.705	41.027		Spillway #2	
95.25	3.096	21.474	45.500			
95.50	3.134	22.253	49.968			
95.75	3.171	23.041	54.431			
96.00	3.209	23.838	67.004			

\*Designates time(s) to dewater have been extrapolated beyond the 50 hour hydrograph limit.

Detailed Discharge Table

## SEDCAD 4 for Windows

			Combined
Elevation	Enh. PerfRiser	Emergency	Total
(ft)	(cfs)	Spillway (cfs)	Discharge
			(cfs)
86.00	0.000	0.000	0.000
86.25	0.000	0.000	0.000
86.50	8.00>0.000	0.000	0.000
86.75	0.174	0.000	0.174
87.00	0.596	0.000	0.596
87.25	1.103	0.000	1.103
87.50	1.395	0.000	1.395
87.75	1.636	0.000	1.636
88.00	1.846	0.000	1.846
88.25	2.034	0.000	2.034
88.50	6.00>2.206	0.000	2.206
88.75	2.508	0.000	2.508
89.00	2.996	0.000	2.996
89.25	3.336	0.000	3.336
89.50	3.623	0.000	3.623
89.75	3.879	0.000	3.879
90.00	4.115	0.000	4.115
90.25	4.336	0.000	4.336
90.50	4.544	0.000	4.544
90.75	4.741	0.000	4.741
91.00	4.930	0.000	4.930
91.25	5.111	0.000	5.111
91.50	5.285	0.000	5.285
91.75	5.454	0.000	5.454
92.00	5.617	0.000	5.617
92.25	5.775	0.000	5.775
92.50	5.929	0.000	5.929
92.75	6.079	0.000	6.079
93.00	6.225	0.000	6.225
93.25	6.367	0.000	6.367
93.50	6.507	0.000	6.507
93.75	6.643	0.000	6.643
94.00	13.773	0.000	13.773
94.25	25.303	0.000	25.303
94.50	38.956	0.000	38.956
94.75	40.558	0.000	40.558
95.00	41.027	0.000	41.027
95.25	41.491	4.010	45.500
95.50	41.949	8.019	49.968
95.75	42.403	12.029	54.431
96.00	42.851	24.153	67.004

<u>Structure #4 (Null)</u>

POI 2 (includes Western Portion of Wetlands)

Stru	SWS	SWS Area	Time of Conc	Musk K	Musk X	Curve	UHS	Peak Discharge	Runoff Volume
π	π	(ac)	(hrs)	(nrs)		Number		(cfs)	(ac-ft)
#3	1	2.520	0.324	0.003	0.254	84.000	TR55	19.65	1.519
	Σ	2.520						19.65	1.519
#1	1	44.210	0.169	0.000	0.000	84.000	TR55	432.70	27.456
	Σ	44.210						432.70	27.456
#4	1	13.440	1.210	0.331	0.126	79.000	TR55	44.53	7.467
	Σ	60.170						67.07	31.252

### Subwatershed Hydrology Detail:

#### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	2. Minimum tillage cultivation	4.62	8.00	173.00	1.070	0.044
		8. Large gullies, diversions, and low flowing streams	1.03	13.00	1,257.00	3.050	0.114
		8. Large gullies, diversions, and low flowing streams	18.76	103.00	549.00	12.990	0.011
#1	1	Time of Concentration:					0.169
#3	1	3. Short grass pasture	33.33	19.00	57.00	4.610	0.003
		8. Large gullies, diversions, and low flowing streams	0.35	7.20	2,046.03	1.770	0.321
#3	1	Time of Concentration:					0.324
#4	1	1. Forest with heavy ground litter	0.19	0.30	154.00	0.110	0.388
		4. Cultivated, straight row	0.08	0.50	656.00	0.240	0.759
		8. Large gullies, diversions, and low flowing streams	0.22	0.70	319.00	1.400	0.063
#4	1	Time of Concentration:					1.210

## Subwatershed Muskingum Routing Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#3	1	6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#3	1	Muskingum K:					0.003
#4	1	8. Large gullies, diversions, and low flowing streams	0.03	0.20	627.00	0.530	0.328
		6. Grassed waterway	1.36	0.30	22.00	1.750	0.003
#4	1	Muskingum K:					0.331

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 3 2-year, 24-hour Storm Event 3.8 inches* 

L.Lotrakul

#### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	2 yr - 24 hr
Rainfall Depth:	3.800 inches

	Su uclure Networking:											
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description						
Null	#4	==>	End	0.000	0.000	Wetlands						

#4 Null

#### Structure Networking C

	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#4	9.280	9.280	12.33	1.38

#### Structure Summary:

#### Structure Detail:

Structure #4 (Null)

Wetlands

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	9.280	0.652	0.000	0.000	79.000	TR55	12.33	1.380
	Σ	9.280						12.33	1.380

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	1. Forest with heavy ground litter	0.65	1.00	154.00	0.200	0.213
		4. Cultivated, straight row	0.28	2.00	727.00	0.460	0.439
#4	1	Time of Concentration:					0.652

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 3 10-year, 24-hour Storm Event 5.8 inches* 

L.Lotrakul

1

#### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

Structure Networking:											
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#4	==>	End	0.000	0.000	Wetlands					

#4 Null

#### Structure Networking C

	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
(ac)		(ac)	(cfs)	(ac-ft)
#4	9.280	9.280	24.31	2.68

#### Structure Summary:

#### Structure Detail:

Structure #4 (Null)

Wetlands

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	9.280	0.652	0.000	0.000	79.000	TR55	24.31	2.681
	Σ	9.280						24.31	2.681

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	1. Forest with heavy ground litter	0.65	1.00	154.00	0.200	0.213
		4. Cultivated, straight row	0.28	2.00	727.00	0.460	0.439
#4	1	Time of Concentration:					0.652

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 3 25-year, 24-hour Storm Event 7.1 inches* 

L.Lotrakul

#### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

Structure Networking:											
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#4	==>	End	0.000	0.000	Wetlands					

#4 Null

#### Structure Networking C

	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume (ac-ft)	
	(ac)	(ac)	(cfs)		
#4	9.280	9.280	32.40	3.58	

#### Structure Summary:

#### Structure Detail:

Structure #4 (Null)

Wetlands

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	9.280	0.652	0.000	0.000	79.000	TR55	32.40	3.581
	Σ	9.280						32.40	3.581

## Subwatershed Hydrology Detail:

## Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	1. Forest with heavy ground litter	0.65	1.00	154.00	0.200	0.213
		4. Cultivated, straight row	0.28	2.00	727.00	0.460	0.439
#4	1	Time of Concentration:					0.652
# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 3 100-year, 24-hour Storm Event 9.3 inches* 

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

Structure Networking:											
Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#4	==>	End	0.000	0.000	Wetlands					

#4 Null

#### Structure Networking C

	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#4	9.280	9.280	46.27	5.15

### Structure Summary:

#### Structure Detail:

Structure #4 (Null)

Wetlands

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#4	1	9.280	0.652	0.000	0.000	79.000	TR55	46.27	5.152
	Σ	9.280						46.27	5.152

### Subwatershed Hydrology Detail:

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#4	1	1. Forest with heavy ground litter	0.65	1.00	154.00	0.200	0.213
		4. Cultivated, straight row	0.28	2.00	727.00	0.460	0.439
#4	1	Time of Concentration:					0.652

## **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 4 2-year, 24-hour Storm Event 3.8 inches* 

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	2 yr - 24 hr
Rainfall Depth:	3.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description							
Null	#1	==>	End	0.000	0.000	Buffer and Grass to POI 4 (South East)							

### Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	12.790	12.790	4.72	2.11

### Structure Summary:

### Structure Detail:

Structure #1 (Null)

Buffer and Grass to POI 4 (South East)

					-	•••			
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	12.790	4.463	0.000	0.000	81.500	TR55	4.72	2.107
	Σ	12.790						4.72	2.107

### Subwatershed Hydrology Detail:

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	0.09	7.00	7,392.00	0.460	4.463
#1	1	Time of Concentration:					4.463

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 4 10-year, 24-hour Storm Event 5.8 inches* 

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	10 yr - 24 hr
Rainfall Depth:	5.800 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description							
Null	#1	==>	End	0.000	0.000	Buffer and Grass to POI 4 (South East)							

### Structure Networking:



	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
	(ac)	(ac)	(cfs)	(ac-ft)
#1	12.790	12.790	9.04	3.97

### Structure Summary:

4

### Structure Detail:

Structure #1 (Null)

Buffer and Grass to POI 4 (South East)

5

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	12.790	4.463	0.000	0.000	81.500	TR55	9.04	3.966
	Σ	12.790						9.04	3.966

### Subwatershed Hydrology Detail:

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	0.09	7.00	7,392.00	0.460	4.463
#1	1	Time of Concentration:					4.463

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 4 25-year, 24-hour Storm Event 7.1 inches* 

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	25 yr - 24 hr
Rainfall Depth:	7.100 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	Buffer and Grass to POI 4 (South East)					

### Structure Networking:



	Immediate Contributing Area	Total Contributing Area	Peak Discharge	Total Runoff Volume
	(ac)	(ac)	(CIS)	(ac-ft)
#1	12.790	12.790	11.96	5.24

### Structure Summary:

### Structure Detail:

Structure #1 (Null)

Buffer and Grass to POI 4 (South East)

5

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	12.790	4.463	0.000	0.000	81.500	TR55	11.96	5.236
	Σ	12.790						11.96	5.236

### Subwatershed Hydrology Detail:

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	0.09	7.00	7,392.00	0.460	4.463
#1	1	Time of Concentration:					4.463

# **Vulcan Orangeburg**

*Post Development for Hydrological Point of Interest 4 100-year, 24-hour Storm Event 9.3 inches* 

L.Lotrakul

### **General Information**

### Storm Information:

Storm Type:	NRCS Type II
Design Storm:	100 yr - 24 hr
Rainfall Depth:	9.300 inches

Туре	Stru #	(flows into)	Stru #	Musk. K (hrs)	Musk. X	Description					
Null	#1	==>	End	0.000	0.000	Buffer and Grass to POI 4 (South East)					

### Structure Networking:



	Immediate Contributing Area (ac)	Total Contributing Area (ac)	Peak Discharge (cfs)	Total Runoff Volume (ac-ft)
#1	12.790	12.790	16.94	7.44

### Structure Summary:

4

### Structure Detail:

Structure #1 (Null)

Buffer and Grass to POI 4 (South East)

5

					-				
Stru #	SWS #	SWS Area (ac)	Time of Conc (hrs)	Musk K (hrs)	Musk X	Curve Number	UHS	Peak Discharge (cfs)	Runoff Volume (ac-ft)
#1	1	12.790	4.463	0.000	0.000	81.500	TR55	16.94	7.441
	Σ	12.790						16.94	7.441

### Subwatershed Hydrology Detail:

### Subwatershed Time of Concentration Details:

Stru #	SWS #	Land Flow Condition	Slope (%)	Vert. Dist. (ft)	Horiz. Dist. (ft)	Velocity (fps)	Time (hrs)
#1	1	6. Grassed waterway	0.09	7.00	7,392.00	0.460	4.463
#1	1	Time of Concentration:					4.463

### **ATTACHMENT 5**

SOIL MAP

#### synterracorp.com



United States Department of Agriculture

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Orangeburg County, South Carolina



### Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

alternative means for communication of program information (Braille, large print, audiotape, etc.) should contact USDA's TARGET Center at (202) 720-2600 (voice and TDD). To file a complaint of discrimination, write to USDA, Director, Office of Civil Rights, 1400 Independence Avenue, S.W., Washington, D.C. 20250-9410 or call (800) 795-3272 (voice) or (202) 720-6382 (TDD). USDA is an equal opportunity provider and employer.

### Contents

Preface	2	
How Soil Surveys Are Made	5	
Soil Map	8	
Soil Map	9	
Legend	10	
Map Unit Legend	11	
Map Unit Descriptions	11	
Orangeburg County, South Carolina	14	
BIB—Blanton sand, 0 to 6 percent slopes	14	
BoB—Bonneau sand, 0 to 4 percent slopes	15	
By—Byars loam	16	
Cx—Coxville sandy loam	17	
Dn—Dunbar sandy loam		
DpA—Duplin loamy sand, 0 to 2 percent slopes	19	
Eo—Elloree loamy sand	20	
GoA—Goldsboro sandy loam, 0 to 2 percent slopes	21	
Ly—Lynchburg fine sandy loam, 0 to 2 percent slopes	22	
Mo—Mouzon fine sandy loam	24	
NoA—Noboco loamy sand, 0 to 2 percent slopes	25	
OcA—Ocilla loamy sand, 0 to 2 percent slopes		
Pa—Pantego fine sandy loam	27	
Ra—Rains sandy loam	28	
Sa—Stallings loamy sand	29	
W—Water	30	
References		

### **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil
scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND				MAP INFORMATION	
Area of Int	erest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:20,000.	
	Soil Map Unit Polygons Soil Map Unit Lines	blygons Very Stony Spot Please rely on the bar scale on each map sh w Wet Spot measurements.	Please rely on the bar scale on each map sheet for map measurements.		
Special I	Soil Map Unit Points Point Features	~	Other Special Line Features	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)	
0 2 *	Blowout Borrow Pit Clay Spot	Transporta	Streams and Canals portation Rails	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more	
◇ ¥	Closed Depression Gravel Pit Gravelly Spot	<b>* * *</b>	Interstate Highways US Routes Major Roads	accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.	
© 1.	Landfill Lava Flow Marsh or swamp	Backgrour	Local Roads nd Aerial Photography	Soil Survey Area: Orangeburg County, South Carolina Survey Area Data: Version 17, Jun 3, 2020	
~ ©	, Mine or Quarry Miscellaneous Water			Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Nov 3, 2019—Nov	
0 ~ +	Perennial Water Rock Outcrop Saline Spot			10, 2019 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background	
 e	Sandy Spot Severely Eroded Spot			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.	
\$ } Ø	Sinkhole Slide or Slip Sodic Spot				

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BIB	Blanton sand, 0 to 6 percent slopes	20.0	2.6%
ВоВ	Bonneau sand, 0 to 4 percent slopes	20.6	2.7%
Ву	Byars loam	41.7	5.5%
Сх	Coxville sandy loam	85.5	11.2%
Dn	Dunbar sandy loam	3.6	0.5%
DpA	Duplin loamy sand, 0 to 2 percent slopes	1.2	0.2%
Ео	Elloree loamy sand	2.8	0.4%
GoA	Goldsboro sandy loam, 0 to 2 percent slopes	296.4	38.8%
Ly	Lynchburg fine sandy loam, 0 to 2 percent slopes	70.5	9.2%
Мо	Mouzon fine sandy loam	31.8	4.2%
NoA	Noboco loamy sand, 0 to 2 percent slopes	32.6	4.3%
OcA	Ocilla loamy sand, 0 to 2 percent slopes	30.9	4.0%
Ра	Pantego fine sandy loam	12.3	1.6%
Ra	Rains sandy loam	77.7	10.2%
Sa	Stallings loamy sand	31.8	4.2%
W	Water	3.6	0.5%
Totals for Area of Interest		763.2	100.0%

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example. An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

# **Orangeburg County, South Carolina**

# BIB—Blanton sand, 0 to 6 percent slopes

## **Map Unit Setting**

National map unit symbol: 4d5r Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Not prime farmland

## **Map Unit Composition**

Blanton and similar soils: 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Blanton**

## Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Sandy and/or loamy marine deposits

## **Typical profile**

A - 0 to 5 inches: sand Bw - 5 to 61 inches: sand Bt1 - 61 to 64 inches: sandy loam Bt2 - 64 to 82 inches: sandy clay loam

## **Properties and qualities**

Slope: 0 to 6 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 30 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Very low (about 3.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Hydric soil rating: No

## BoB—Bonneau sand, 0 to 4 percent slopes

#### Map Unit Setting

National map unit symbol: 4d5t Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

## **Map Unit Composition**

Bonneau and similar soils: 90 percent Minor components: 4 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Bonneau**

## Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Loamy marine deposits

## **Typical profile**

A - 0 to 8 inches: sand E - 8 to 35 inches: loamy sand Bt1 - 35 to 69 inches: sandy clay loam Bt2 - 69 to 80 inches: sandy clay

## Properties and qualities

Slope: 0 to 4 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)
Depth to water table: About 42 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 6.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Hydric soil rating: No

#### **Minor Components**

#### Coxville

Percent of map unit: 2 percent

Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Blanton

Percent of map unit: 2 percent Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## By—Byars loam

## Map Unit Setting

National map unit symbol: 4d5v Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

Byars and similar soils: 95 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Byars**

## Setting

Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Parent material: Clayey marine deposits

## **Typical profile**

A - 0 to 9 inches: loam Btg - 9 to 45 inches: clay Btg - 45 to 63 inches: clay loam BCg - 63 to 70 inches: sandy loam

## **Properties and qualities**

Slope: 0 to 2 percent Depth to restrictive feature: More than 80 inches Drainage class: Very poorly drained Runoff class: Negligible Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr) Depth to water table: About 0 inches Frequency of flooding: None Frequency of ponding: Occasional Available water capacity: High (about 9.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: C/D Hydric soil rating: Yes

## **Minor Components**

## Coxville

Percent of map unit: 2 percent Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

# Cx—Coxville sandy loam

## **Map Unit Setting**

National map unit symbol: 4d5x Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

## Map Unit Composition

*Coxville and similar soils:* 95 percent *Minor components:* 2 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

## **Description of Coxville**

## Setting

Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Parent material: Clayey marine deposits

#### **Typical profile**

A - 0 to 5 inches: sandy loam Btg - 5 to 60 inches: clay

## **Properties and qualities**

Slope: 0 to 2 percent

#### **Custom Soil Resource Report**

Depth to restrictive feature: More than 80 inches Drainage class: Poorly drained Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr) Depth to water table: About 0 to 12 inches Frequency of flooding: None Frequency of ponding: None Available water capacity: High (about 9.5 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: C/D Hydric soil rating: Yes

#### **Minor Components**

#### Rains

Percent of map unit: 2 percent Landform: Depressions, marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

## Dn—Dunbar sandy loam

#### Map Unit Setting

National map unit symbol: 4d60 Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

*Dunbar and similar soils:* 96 percent *Minor components:* 2 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Dunbar**

#### Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Clayey marine deposits

## **Typical profile**

*Ap - 0 to 8 inches:* sandy loam *Bt - 8 to 26 inches:* clay loam *Btg - 26 to 70 inches:* clay

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)
Depth to water table: About 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: High (about 9.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: C/D Hydric soil rating: No

### **Minor Components**

## Coxville

Percent of map unit: 2 percent Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

# DpA—Duplin loamy sand, 0 to 2 percent slopes

## **Map Unit Setting**

National map unit symbol: 4d61 Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: All areas are prime farmland

## Map Unit Composition

*Duplin and similar soils:* 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Duplin**

#### Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Clayey marine deposits

## **Typical profile**

Ap - 0 to 6 inches: loamy sand E - 6 to 13 inches: loamy sand Bt - 13 to 38 inches: sandy clay Btg - 38 to 62 inches: clay

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)
Depth to water table: About 24 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 7.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: C Hydric soil rating: No

# Eo—Elloree loamy sand

## Map Unit Setting

National map unit symbol: 4d62 Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Elloree and similar soils:* 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Elloree**

#### Setting

Landform: Flood plains Landform position (three-dimensional): Tread *Down-slope shape:* Linear *Across-slope shape:* Linear *Parent material:* Loamy fluviomarine deposits

## **Typical profile**

A - 0 to 6 inches: loamy sand Eg - 6 to 23 inches: sand Btg - 23 to 42 inches: sandy loam BCg - 42 to 69 inches: loamy sand Cg - 69 to 80 inches: sandy loam

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: OccasionalNone
Frequency of ponding: None
Available water capacity: Moderate (about 6.2 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6w Hydrologic Soil Group: A/D Hydric soil rating: Yes

# GoA—Goldsboro sandy loam, 0 to 2 percent slopes

## Map Unit Setting

National map unit symbol: 4d66 Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: All areas are prime farmland

## **Map Unit Composition**

*Goldsboro and similar soils:* 96 percent *Minor components:* 2 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Goldsboro**

## Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Loamy marine deposits

## **Typical profile**

Ap - 0 to 8 inches: sandy loam E - 8 to 16 inches: sandy loam Bt - 16 to 45 inches: sandy clay loam Btg - 45 to 68 inches: sandy clay loam

## Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 24 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 7.3 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: C Ecological site: R153AY001GA - Loamy Rise, Moderately Wet Hydric soil rating: No

## **Minor Components**

## Rains

Percent of map unit: 2 percent Landform: Depressions, marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

# Ly—Lynchburg fine sandy loam, 0 to 2 percent slopes

## Map Unit Setting

National map unit symbol: 2tzkm Elevation: 0 to 280 feet Mean annual precipitation: 45 to 52 inches Mean annual air temperature: 64 to 65 degrees F Frost-free period: 250 to 310 days Farmland classification: Prime farmland if drained

## Map Unit Composition

*Lynchburg and similar soils:* 92 percent *Minor components:* 8 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Lynchburg**

#### Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Loamy marine deposits

#### **Typical profile**

Ap - 0 to 7 inches: fine sandy loam Bt - 7 to 13 inches: sandy clay loam Btg - 13 to 62 inches: sandy clay loam BCg - 62 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 4.9 inches)

### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: B/D Hydric soil rating: No

## **Minor Components**

#### Goldsboro

Percent of map unit: 3 percent Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Coxville, drained

Percent of map unit: 3 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread Down-slope shape: Linear, concave Across-slope shape: Linear, concave Hydric soil rating: Yes

#### Ocilla

Percent of map unit: 2 percent Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Ecological site: R153AY001GA - Loamy Rise, Moderately Wet Hydric soil rating: No

# Mo—Mouzon fine sandy loam

## Map Unit Setting

National map unit symbol: 4d6g Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Not prime farmland

## Map Unit Composition

Mouzon and similar soils: 90 percent Minor components: 4 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Mouzon**

## Setting

Landform: Flood plains Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Clayey fluviomarine deposits

## **Typical profile**

A - 0 to 4 inches: fine sandy loam Eg - 4 to 11 inches: loamy sand Btg - 11 to 50 inches: sandy clay loam Cg - 50 to 74 inches: sandy loam

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: FrequentNone
Frequency of ponding: None
Available water capacity: Moderate (about 7.1 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6w Hydrologic Soil Group: C/D Hydric soil rating: Yes

#### **Minor Components**

#### Lumbee

Percent of map unit: 2 percent Landform: Flood plains Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

## Johns

Percent of map unit: 2 percent Landform: Stream terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

# NoA—Noboco loamy sand, 0 to 2 percent slopes

## **Map Unit Setting**

National map unit symbol: 4d6l Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: All areas are prime farmland

## Map Unit Composition

Noboco and similar soils: 95 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Noboco**

#### Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Loamy marine deposits

## **Typical profile**

Ap - 0 to 7 inches: loamy sand E - 7 to 13 inches: loamy sand Bt - 13 to 72 inches: sandy clay loam

## **Properties and qualities**

*Slope:* 0 to 2 percent *Depth to restrictive feature:* More than 80 inches

Drainage class: Well drained Runoff class: Low Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr) Depth to water table: About 30 inches Frequency of flooding: None Frequency of ponding: None Available water capacity: Moderate (about 8.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 1 Hydrologic Soil Group: C Hydric soil rating: No

## **Minor Components**

#### Coxville

Percent of map unit: 2 percent Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## OcA—Ocilla loamy sand, 0 to 2 percent slopes

## Map Unit Setting

National map unit symbol: 4d6n Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

*Ocilla and similar soils:* 97 percent *Minor components:* 2 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Ocilla**

## Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Loamy marine deposits

#### **Typical profile**

A - 0 to 3 inches: loamy sand

*E - 3 to 24 inches:* loamy sand *Bt - 24 to 37 inches:* sandy clay loam *Btg - 37 to 70 inches:* sandy clay loam

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 5.6 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: B/D Ecological site: R153AY001GA - Loamy Rise, Moderately Wet Hydric soil rating: No

## **Minor Components**

## Pelham

Percent of map unit: 2 percent Landform: Depressions, marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

# Pa—Pantego fine sandy loam

## Map Unit Setting

National map unit symbol: 4d6s Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

## **Map Unit Composition**

Pantego and similar soils: 96 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Pantego**

#### Setting

Landform: Depressions Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Parent material: Loamy marine deposits

#### **Typical profile**

A - 0 to 12 inches: fine sandy loam Btg1 - 12 to 59 inches: sandy clay loam Btg2 - 59 to 67 inches: sandy clay

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: High (about 9.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: B/D Hydric soil rating: Yes

## **Minor Components**

## Rains

Percent of map unit: 2 percent Landform: Marine terraces, depressions Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

## Ra—Rains sandy loam

## Map Unit Setting

National map unit symbol: 4d6v Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

*Rains and similar soils:* 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Rains**

#### Setting

Landform: Depressions, marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Loamy marine deposits

#### **Typical profile**

A - 0 to 5 inches: sandy loam Eg - 5 to 12 inches: sandy loam Btg - 12 to 70 inches: sandy clay loam

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 7.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: B/D Hydric soil rating: Yes

## Sa—Stallings loamy sand

## Map Unit Setting

National map unit symbol: 4d6x Elevation: 50 to 400 feet Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F Frost-free period: 225 to 265 days Farmland classification: Prime farmland if protected from flooding or not frequently flooded during the growing season

## Map Unit Composition

Stallings and similar soils: 96 percent Minor components: 2 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Stallings**

#### Setting

Landform: Marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Parent material: Loamy marine deposits

#### **Typical profile**

A - 0 to 5 inches: loamy sand E - 5 to 11 inches: loamy sand Bt - 11 to 52 inches: sandy loam Btg - 52 to 68 inches: sandy clay loam

## **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 5.95 in/hr)
Depth to water table: About 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 7.6 inches)

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: A/D Hydric soil rating: No

## Minor Components

## Rains

Percent of map unit: 2 percent Landform: Depressions, marine terraces Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: Yes

## W-Water

## Map Unit Setting

National map unit symbol: 4d71 Mean annual precipitation: 44 to 55 inches Mean annual air temperature: 61 to 70 degrees F *Frost-free period:* 225 to 265 days *Farmland classification:* Not prime farmland

# Map Unit Composition

Water: 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

# References

American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.

American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.

Cowardin, L.M., V. Carter, F.C. Golet, and E.T. LaRoe. 1979. Classification of wetlands and deep-water habitats of the United States. U.S. Fish and Wildlife Service FWS/OBS-79/31.

Federal Register. July 13, 1994. Changes in hydric soils of the United States.

Federal Register. September 18, 2002. Hydric soils of the United States.

Hurt, G.W., and L.M. Vasilas, editors. Version 6.0, 2006. Field indicators of hydric soils in the United States.

National Research Council. 1995. Wetlands: Characteristics and boundaries.

Soil Survey Division Staff. 1993. Soil survey manual. Soil Conservation Service. U.S. Department of Agriculture Handbook 18. http://www.nrcs.usda.gov/wps/portal/ nrcs/detail/national/soils/?cid=nrcs142p2\_054262

Soil Survey Staff. 1999. Soil taxonomy: A basic system of soil classification for making and interpreting soil surveys. 2nd edition. Natural Resources Conservation Service, U.S. Department of Agriculture Handbook 436. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\_053577

Soil Survey Staff. 2010. Keys to soil taxonomy. 11th edition. U.S. Department of Agriculture, Natural Resources Conservation Service. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2 053580

Tiner, R.W., Jr. 1985. Wetlands of Delaware. U.S. Fish and Wildlife Service and Delaware Department of Natural Resources and Environmental Control, Wetlands Section.

United States Army Corps of Engineers, Environmental Laboratory. 1987. Corps of Engineers wetlands delineation manual. Waterways Experiment Station Technical Report Y-87-1.

United States Department of Agriculture, Natural Resources Conservation Service. National forestry manual. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/ home/?cid=nrcs142p2 053374

United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. http://www.nrcs.usda.gov/wps/portal/nrcs/ detail/national/landuse/rangepasture/?cid=stelprdb1043084

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. http://www.nrcs.usda.gov/wps/portal/ nrcs/detail/soils/scientists/?cid=nrcs142p2\_054242

United States Department of Agriculture, Natural Resources Conservation Service. 2006. Land resource regions and major land resource areas of the United States, the Caribbean, and the Pacific Basin. U.S. Department of Agriculture Handbook 296. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/? cid=nrcs142p2\_053624

United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE\_DOCUMENTS/nrcs142p2\_052290.pdf